

26 July 2021

ASX: TMG

## ASX ANNOUNCEMENT

# Maiden Indicated Resource for Lake Throssell Sulphate of Potash Project

*Indicated Resource is based on results of recent trench pump trials of the Surficial Aquifer resource and will underpin the Scoping Study due for completion in late Q3*

### Highlights

- Maiden Indicated Mineral Resource estimate of 1.9Mt of drainable Sulphate of Potash (**SOP**) at 4,985mg/L potassium (**K**) (or 11.1kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>), with 13% of the total Mineral Resource now in the higher-confidence Indicated status
- Total Mineral Resource of 14.3Mt of drainable SOP at 4,665mg/L potassium (or 10.4 kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>)
- Multiple trench pumping tests have demonstrated the geological continuity of brine grade and extraction from the surficial aquifer
- Over 95% of the mineralised blocks from the top 6 metres of the surficial aquifer resource model converted to Indicated status
- Further work programs planned to improve the resource confidence of the basal aquifer and remaining palaeovalley to a depth of 100-150 metres
- High conversion expected from Indicated Mineral Resources to Probable Ore Reserves
- Indicated Resource provides basis for the initial project payback period in the ongoing Scoping Study, due for completion late this quarter

**Trigg Mining Limited (ASX: TMG) (Trigg or the Company)** is pleased to announce another key milestone in its aim of developing a new long-life SOP production hub in the Laverton district of Western Australia, with the estimation of a maiden Indicated Mineral Resource for its high-grade Lake Throssell Potash Project near Laverton in Western Australia.

**A Drainable Indicated Mineral Resource of 1.9Mt SOP at 4,985mg/L K** (or 11.1kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) has been estimated based on the results of the recent trench pump trials of the surficial aquifer resource announced to the ASX on 7 July 2021.

As a result of this Mineral Resource Estimate (MRE) upgrade, 13% of the previously announced total MRE of 14.3Mt of drainable SOP at 4,665mg/L potassium (or 10.4 kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) is now in the higher-confidence Indicated category and available for conversion to Ore Reserves.

The Exploration Target has also been updated, indicating strong potential to expand this MRE. The new **Exploration Target**, in addition to the MRE, has been defined as a range of **2.6 - 9.4Mt at 9.1 - 10.0kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>**. The potential quantity and grade of the Exploration Target is conceptual in nature. There has been insufficient exploration in these areas to estimate a Mineral Resource. It is uncertain if further exploration will result in the estimation of a Mineral Resource.

The Exploration Target is based on the results of exploration activities undertaken to-date on granted tenement E38/3065, encompassing a strike length of ~36km of the interpreted palaeovalley. An additional ~34km of strike length is extrapolated into tenement applications E38/3544, E38/3483, E38/3458 and E38/3537, which are considered to host similar geology and brine characteristics.

**Trigg Mining’s Managing Director, Keren Paterson, said:** “This is another great result by our team, which puts Trigg Mining front and centre of the new-generation SOP industry in Western Australia.

Having delivered our maiden Inferred Resources just over two months ago, we have moved rapidly to estimate a high-quality Indicated Resource that will provide the basis for the initial payback period to underpin the Scoping Study that is currently underway and due for completion later this quarter.

In addition to improving our confidence in the current Mineral Resource, we have also demonstrated continued upside potential with an updated Exploration Target of 2.6 - 9.4Mt of SOP, encompassing tenements to the north and south which are awaiting grant.

We expect to convert additional tonnes to Indicated status next year as we progress work on the deeper portions of the resource and further expand our overall inventory with further drilling. However, having a maiden Indicated Resource allows us to progress our economic evaluation of Lake Throssell to the next stage, and commence initial discussions with potential off-takers and financiers.

Together with our Lake Rason Project, we now have a high degree of confidence that we have a large and potential multi-decade, long life potash project in Western Australia.”

### Lake Throssell Project

The Lake Throssell Potash Project is 100%-owned and operated by Trigg Mining and lies approximately 170km north-east of Laverton, situated on a granted Exploration Licence (E38/3065). Trigg has a total of 1,084km<sup>2</sup> of exploration tenure granted or pending approval across Lake Throssell.

The extensive palaeovalley system has been identified through 200-line kilometres of gravity surveying. The Mineral Resource Estimate is based on 80 air-core and rotary drill holes for a total drill depth of 5,720 metres (see Figure 1).

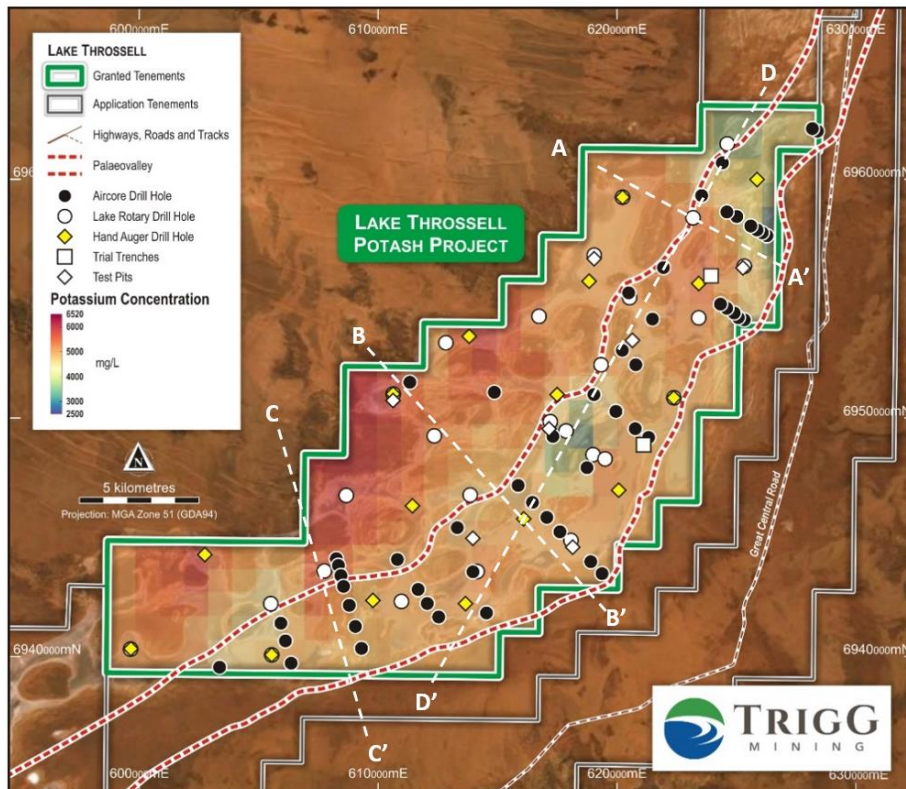


Figure 1: Drill collar map for the Lake Throssell Potash Project

A successful brine pumping trial was completed at Lake Throssell from two 100m long trenches over ten days and seven test pits (ASX announcement on 7 July 2021). This recent work has improved the confidence of the lake surface surficial aquifer to Indicated status.

## Overview of Updated Mineral Resource Estimate

The updated Mineral Resource for the Lake Throssell Potash Project is presented in Table 1 below and has been reported in accordance with the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves, (JORC Code 2012). The updated Mineral Resource Estimate has increased the overall geological confidence of the Lake Throssell Project and enables mining studies to be undertaken. An executive summary of this Mineral Resource Estimate follows this section, and the JORC Table 1 is included in Appendix 2 to this announcement.

The total contained brine SOP mass within the palaeovalley is 75.7Mt compared to the reported drainable brine volume of 14.3Mt. The drainable brine volume represents the amount of SOP that can be abstracted from the deposit under normal pumping conditions. For economic production, the drainable brine volume is the volume that can be abstracted from the deposit.

The basis of this updated Mineral Resource estimate is the inclusion of test pumping data for the lake surface sequence of the surficial aquifer, which has allowed conversion from Inferred Mineral Resources to Indicated Mineral Resources.

The Indicated Resource represents the upper 6 metres of the surficial aquifer, which has a total depth or thickness of approximately 25 metres. The conversion to Indicated Mineral Resources is an important step as this classification can be incorporated into mine plans and financial analysis of the project for the Scoping Study.

Table 1: Lake Throssell Mineral Resources July 2021

Resource Domain	Mineral Resource Category	Drainable Brine Volume (10 <sup>6</sup> m <sup>3</sup> )	Potassium (K) Grade (mg/L)	Potassium (K) Mass (Mt)	Sulphate (SO <sub>4</sub> ) Mass (Mt)	Equiv. SOP Grade (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Drainable Brine Equiv. SOP Mass (Mt)	Total Brine Equiv. SOP Mass (Mt)
Surficial Aquifer	Indicated	170	4,985	0.9	3.8	11.1	1.9	4.5
Surficial Aquifer	Inferred	310	4,605	1.4	6.8	10.3	3.2	13.5
Confining Layer	Inferred	350	4,595	1.6	8.1	10.2	3.6	40.6
Basal Aquifer	Inferred	545	4,645	2.5	12.7	10.4	5.6	17.2
Total Mineral Resource		1,375	4,665	6.4	31.4	10.4	14.3	75.7

Note: Errors may be present due to rounding. Approximately 2.90Mt of the Inferred Drainable SOP Mass is present in Exploration Licence Applications E38/3544, E38/3483, E38/3458, and E38/3537.

## Geological Summary

The geology is consistent with other lakes and palaeovalley sequences in the region. Figure 2 shows a typical geological cross-section of the palaeovalley. In the shallow sediments there is an evaporite surface, dominated by gypsum, underlain by more clayey dominated sequences with occasional thin granular and calcrete zones.

These superficial lithologies lie on top of a thick sequence of stiff lacustrine clay, which acts as a regionally confining aquitard layer with very low vertical hydraulic conductivity, meaning it hydraulically separates the shallow sediments of the palaeovalley from the basal aquifer sediments.

Beneath the lacustrine (ancient lake) clay sequence is a fine to medium grained basal sand with silty and clayey bands of fluvial origin between Eocene and Pliocene age. At the base of this fluvial system is the contact with the Permian age Paterson Formation, a palaeosurface that represents up to

200 million years of weathering, erosion and deposition. The contact is present in the base of the palaeovalley, and the Paterson Formation is a fluvial glacial deposit represented in fresh bedrock as dark to light grey poorly sorted siltstone, mudstone, sandstone and quartzite, with conglomerate beds.

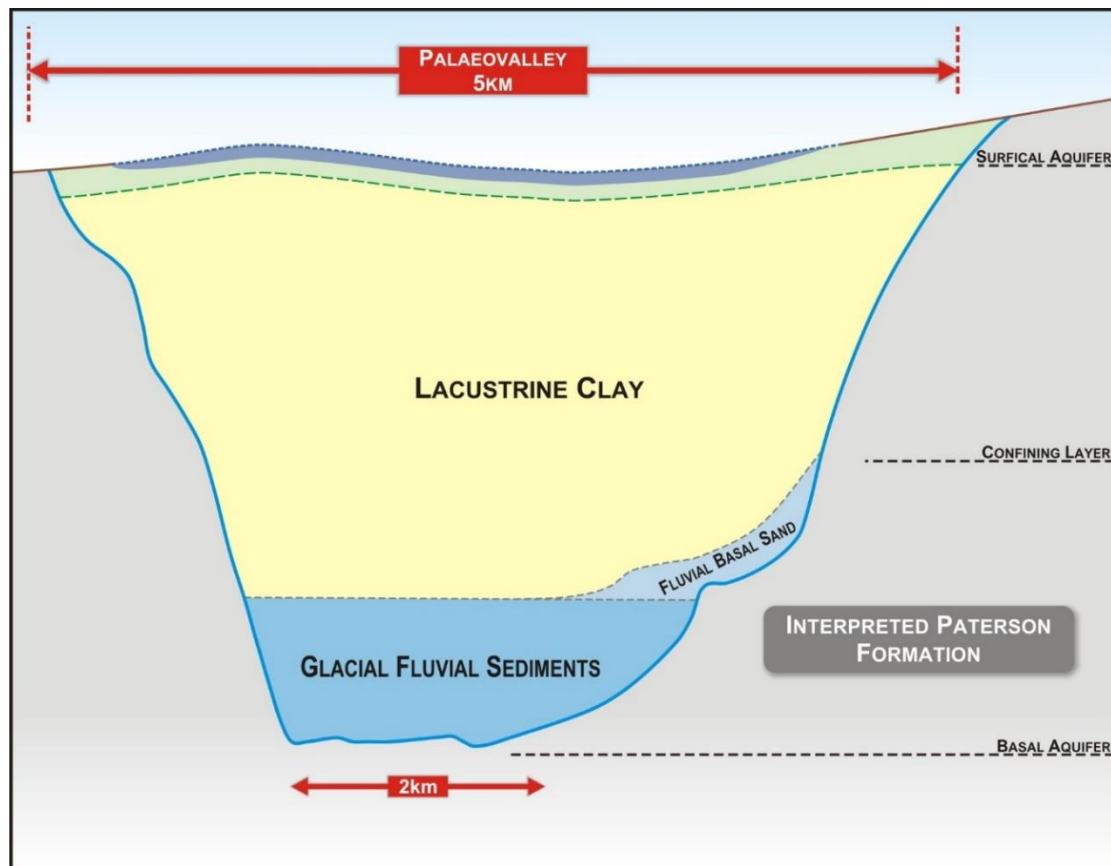


Figure 2: Typical geological cross section of the Lake Throssell paleochannel

### Hydrogeological Domains

The salt lake acts as a point of discharge for the regional groundwater system. Groundwater flow in the shallow sediments within the lake's catchment flows towards the lake surface where evaporation is dominant and there is a net loss to the system making the groundwater hypersaline in nature.

There are three main mineralised domains within the resource. The upper surficial aquifer is typically 25 metres in depth near the lake surface and will be the main source of brine during initial production by constructing a trench network to extract brine from these trenches. The surficial aquifer lies on top of a thick sequence of stiff lacustrine clay, which acts as a confining layer that hydraulically separates the shallow sediments of the palaeovalley from the basal aquifer sediments. The basal aquifer consists of the Eocene fluvial sediments, Permian glacial fluvial sediments and weather basement or saprolite. The brine resource is confined within a Permian basement.

The aquifer potential of each of the stratigraphic layers and an indication of their potential for brine abstraction requires trench pumping trials or test bores trials of each mineralised aquifer domain to increase the Resource confidence and confirm their extraction potential. This has been completed for the upper 6-8 metres of the surficial aquifer resulting in this component of the Inferred Resource being updated to Indicated status.

Typical cross sections of the palaeovalley resource block model are shown in Figure 3, Figure 4 and Figure 5. The plan view locations of these cross sections are shown in Figure 1 (including A-A', B-B' and C-C') and highlights the palaeovalley is typically 100-150 metres in depth with the surficial aquifer normally present from less than one metre from surface.

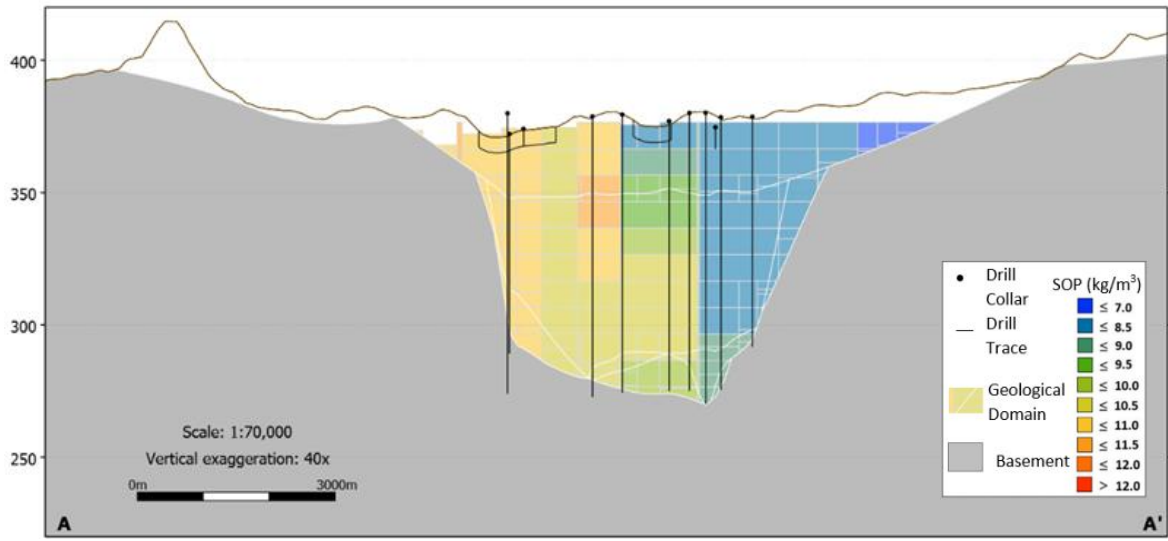


Figure 3: Cross section of resource block model from A-A'

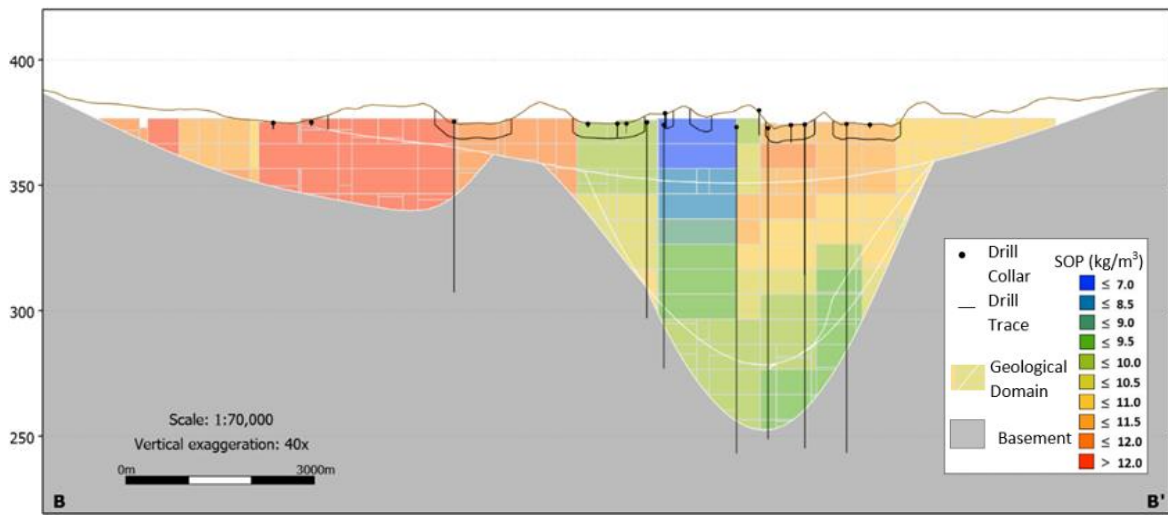


Figure 4: Cross section of resource block model from B-B'

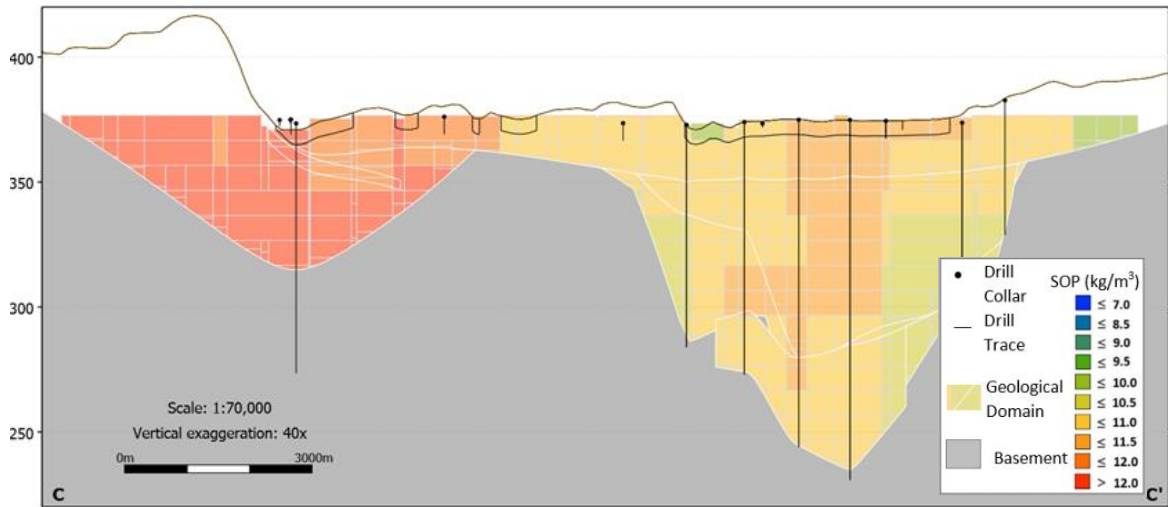


Figure 5: Cross section of resource block model from C-C'

A long section of the Lake Throssell resource is provided in the MRE summary report attached to this announcement. The geological continuity of brine grade and lithology will result in a high conversion of the resource to Indicated Mineral Resources once the Company conducts further pump tests.

### Exploration Target

The Exploration Target is an estimate of the exploration potential of a mineral deposit, Table 2. In a brine hosted deposit, the Exploration Target determines a lower and upper estimate by varying the geological extent, drainable porosity, and brine grade within reasonable bounds based upon the information available.

The geological extent (area and thickness) is determined from a combination of the modelled geological, the gravity model, the mapped outcropping geology and the conceptual model of regionally described palaeovalley systems.

Islands on the lake surface have been removed from the lake surface and alluvial clay sediment volume calculation. Brine grade range is based on the average brine grades from the Resource Tables, with the upper and lower estimates factored for the pending tenements where no data is presently available.

The Exploration Target encompasses the granted tenement E38/3065 and the surrounding pending tenements currently under application. There has been no work completed on the pending tenements meaning that all estimates are based upon reasonable extrapolation from the work completed on E38/3065. At the time of reporting Trigg sees no reason why these tenements will not be granted in the future.

Table 2: Lake Throssell Exploration Target

Resource Domain	Thickness (m)	Area (km <sup>2</sup> )	Sediment Volume (10 <sup>6</sup> m <sup>3</sup> )	Specific Yield (-)	Drainable Brine (10 <sup>6</sup> m <sup>3</sup> )	K Grade (mg/L)	K Mass (Mt)	Equiv. SOP Grade (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Drainable Brine SOP Mass (Mt)
Surficial Aquifer	19	70	656	0.09	61	3,739	0.2	8.3	0.5
Confining Layer	60	68	4,050	0.03	122	4,356	0.5	9.7	1.2
Basal Aquifer	20	144	1,101	0.10	106	3,961	0.4	8.8	0.9
Total Lower Estimate		282	5,807		288	4,081	1.2	9.1	2.6
Surficial Aquifer	26	88	1,156	0.12	134	4,526	0.6	10.1	1.4
Confining Layer	70	90	6,300	0.05	315	4,740	1.5	10.6	3.3
Basal Aquifer	35	269	3,469	0.14	496	4,277	2.1	9.5	4.7
Total Upper Estimate		447	10,925		945	4,466	4.2	10.0	9.4

Note: Errors may be present due to rounding, approximately 2.45 Mt in the lower estimate and 8.76 Mt in the upper estimate of equivalent SOP is present in Exploration Licence Applications E38/3544, E38/3483, E38/3458 and E38/3537. SOP is calculated by multiplying potassium by 2.23.

The potential quantity and grade of the Exploration Target is conceptual in nature. There has been insufficient exploration in these areas to estimate a Mineral Resource. It is uncertain if further exploration will result in the estimation of a Mineral Resource.

## Next Steps

The completion of the Scoping Study for Lake Throssell and installation of test production bores to improve the resource confidence level of the basal aquifer units is high priority for the Company.

The lower aquifer will be geophysically logged to confirm aquifer properties to determine its permeability and specific yield to allow further resource upgrades and support ongoing economic evaluation and development of the Lake Throssell Project after completion of the Scoping Study.

This announcement was authorised to be given to ASX by the Board of Directors of Trigg Mining Limited.



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## Competent Person Statement

The information in this announcement that relates to the Exploration Results, Mineral Resource estimate and Exploration Target is based upon information compiled by Mr Adam Lloyd, who is employed by Aquifer Resources Pty Ltd, an independent consulting company. Mr Lloyd is a Member of the Australian Institute of Geoscientists and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and the activity to which is being undertaking to qualify as a Competent Person for reporting of Exploration Results, Mineral Resources and Ore Reserves as defined in the 2012 edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Lloyd consents to the inclusion in the announcement of the matters based upon the information in the form and context in which it appears.



## Executive Summary

The Lake Throssell Potash Project is 100% owned and operated by Trigg Mining and lies approximately 170km north-east of Laverton, situated on a granted Exploration Licence (E38/3065). Trigg has a total of 1,084km<sup>2</sup> of exploration tenure granted or pending approval across Lake Throssell.

Trigg Mining engaged Aquifer Resources to complete a Mineral Resource Estimate of the Lake Throssell Project. This Mineral Resource Summary Report provides details on the data and methodology used in determining the updated Mineral Resource.

The basis of the updated Mineral Resource is the inclusion of test pumping data for the lake surface surficial aquifer, which has allowed conversion from Inferred Mineral Resources to Indicated Mineral Resources.

## Summary of Exploration

Exploration to date at the Lake Throssell SOP Project has comprised the following programs:

- Lake surface hand auger – 16 drill holes
- Gravity Surveys – 200 line-km
- Heli-supported rotary drilling – 26 drill holes
- Air-core drilling (both on and off lake) – 54 drill holes
- 355 brine assay samples from a total of 5,720m of drilling
- 62 Particle Size Distribution (PSD) analysis to determine drainable porosity
- 18 Lexan-tube core samples taken from the lake sediments
- 2 ten days pumping tests on 100m trial trenches, and
- 7 short term pumping tests on test pits

All drill-holes and surface excavations completed to date are presented in Figure 1 and the following sections are a summary of each of the programs.

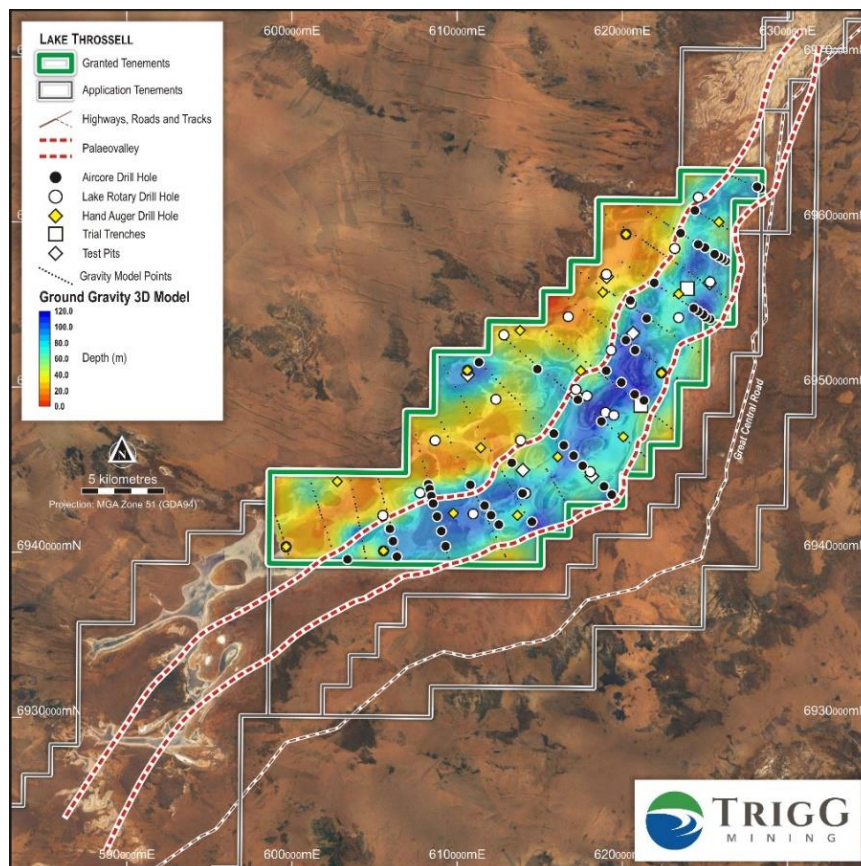


Figure 1: Lake Throssell investigation locations

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## Surficial Aquifer

### Hand Auger Drilling and Sampling

A preliminary lake surface auger program was completed in December 2019 (ASX announcement 16 December 2019) to give an indication of brine grade in the shallow lake sediments. A total of 16 auger holes up to 1.2m in depth were completed.

The holes encountered a typical lake surface sequence, dominated by gypsum with silt and clay, with brine at approximately 0.3m below ground level (bgl). Brine samples were obtained from each hole between 0.3m and the end-of-hole.

The collar locations are presented in Figure 1 and the brine assays and associated geological descriptions are presented in Appendix 1.

### Rotary Auger Drilling and Sampling

The program was completed in July 2020 using a heli-supported rotary auger rig targeting the top sequence of lake surface sediments to a maximum depth of 10m (ASX announcement 10 August 2020). The program obtained brine samples and core samples for porosity testing over the entire playa-lake surface, consisting of 26 drill holes for a total of 86m of core and 77 brine samples. Drill-hole locations are presented in Figure 1.

The program encountered gypsum dominated sandy silt and clay in the top 5m. The gypsum layers were up to 0.2m thick and often associated with good to very good brine in-flow rates, inferring that these zones were more highly permeable.

Minor sand and gravel layers were also identified in three holes, with one hole (LTAG19) containing a clay/silt supported sand interval of at least 1.3m with rounded pebbles. A more clay-dominated sequence is present below 5m, with less gypsum and increasing density.

As part of the program, two holes were designed to test the characteristics of the surficial sequence within the islands (LTAG04 and LTAG05). Drilling and brine analysis confirming a lack of brine flow and more dilute brine, inferring lower permeability and lower grade brine is present within these areas.

Core samples were obtained throughout drilling using Lexan tubes for laboratory sampling and analysis of porosity and permeability.

Brine samples were obtained during the program by bailing the hollow stem of the auger when open to a known interval to provide a representative sample. A summary of collar locations, hole depths, encountered geology and brine analysis is presented in Appendix 1.

### Lake Surface Test Pumping

The program was completed with the aim of estimating the aquifer properties, including drainable porosity (specific yield) and hydraulic conductivity (vertical and horizontal), for the upper section of the lake surface aquifer by test pumping the aquifer.

The program consisted of two trial trenches and seven test pits distributed across the lake. The trenches were 100m long and were surrounded on all sides by a number of monitoring pits. Whilst the test pits consisted of one small trench and one adjacent monitoring pit. All excavations were completed with a 15-tonne amphibious excavator that was able to excavate to depths of between 3m and 4.5m.

The trial trenches were pumped until water levels in the majority of monitoring pits had stabilized – which was between 10 and 11 days in both cases. Test pits consisted of a small pumping trench between 6 and 9m long with an adjacent monitoring pit. Test pits were de-watered and the brine

level draw-down and recovery rates were monitored. Throughout all testing brine levels, flow rate and brine quality was frequently monitored.

Trench locations and dimensions are presented in Figure 1 and Table 1. An example of the 100m long trial trench and monitoring pit network is shown in Figure 2. A test pit excavation is shown in Figure 3, with layering evident close to surface and becoming more clayey with depth.



Figure 2: Trial Trench one with surrounding monitoring pits



Figure 3: Test pumping of a test pit excavation

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The lake surface to 2m below the ground level is more heavily dominated by gypsum, with clayey horizons dominant to the base of the excavation, intermixed with silty zones. The large excavation provided an opportunity to observe the layered nature of the sequence, how the walls stood up and the brine inflow horizons associated with gypsum dominated layers.

The test pumping data has been analysed using local scale numerical models in groundwater modelling software FEFLOW. The models were calibrated to the brine level draw-down and recovery by changing the hydraulic conductivity (horizontal and vertical) and specific yield of the aquifer to obtain an acceptable fit between the measured data and the simulation. Calibration was achieved by a combination of manual and automated iterations. An example of the trench pumping data and calibration simulation is provided in Figure 4, Figure 5 and Figure 6.

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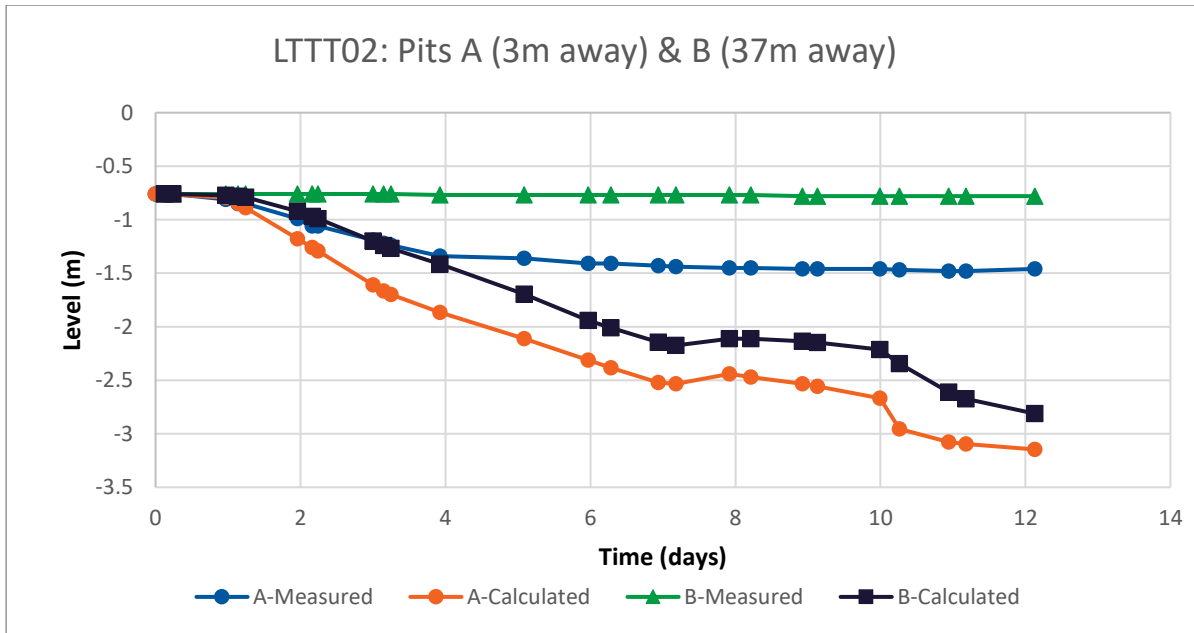


Figure 4: Test pumping measured response and modelling (calculated)

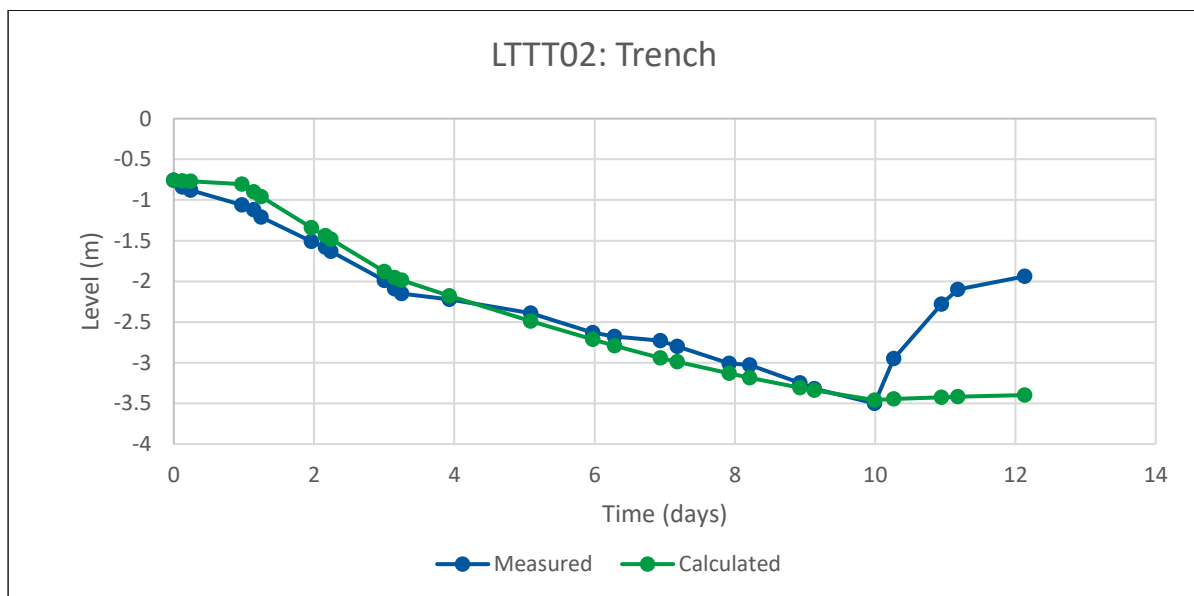


Figure 5: Test pumping measured response and modelling (calculated)

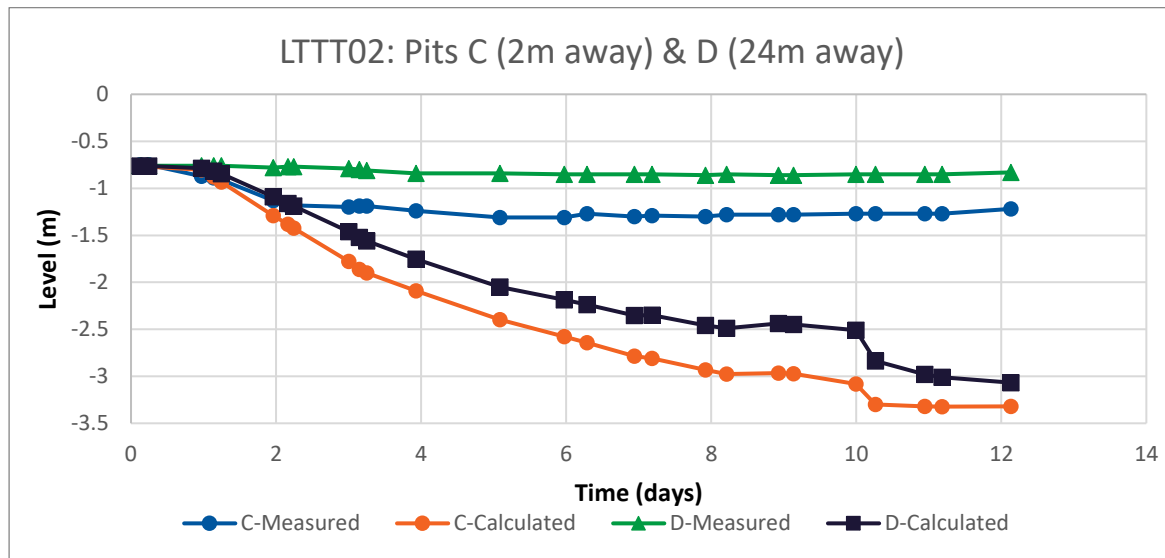


Figure 6: Test pumping measured response and modelling (calculated)

The final aquifer property results from the modelling are highly variable, confirming the highly heterogeneous nature of the layered lake surface aquifer. Specific yield results varied between 0.01 (stiff clay) and 0.4 (the maximum possible related to gypsum evaporite sequences).

Hydraulic conductivity derived from the modelling ranged between 0.2 meters per day (m/d) (stiff clay) and 340m/d (gypsum dominated flow). Hydraulic conductivity was also estimated using distance drawdown analysis for the two trial trenches, these results indicated values of 4.8 and 7.8m/d, which compare favourably to the weighted average of the test pumping results (13.9m/d). The trench pumping results are presented in detail in Table 1.

Table 1: Trench locations and pumping results from modelling

ID	Type	Easting	Northing	Length (m)	Depth (m)	Max Draw-down (m)	Pumping Duration	Average Pumping Rate (L/s)	Hydraulic Conductivity (m/d)	Specific Yield (-)
LTTT01	Trial Trench	623935	6955953	100	4.5	1.9	10 Days	1.0	1.5	0.40
LTTT02	Trial Trench	621117	6948873	100	4.5	2.6	11 Days	1.2	0.5	0.40
LTTT03	Test Pit	619044	6956671	6.5	3.7	2.4	2 Hours	1.2	0.2	0.01
LTTT04	Test Pit	625277	6956289	8.3	3	1.9	3 Hours	2.1	0.8	0.02
LTTT05	Test Pit	617157	6949545	6.3	4	2.8	2.5 Hours	1.4	0.6	0.01
LTTT06	Test Pit	620646	6953250	8.6	3	1.9	1.5 Hours	1.7	1.9	0.05
LTTT07	Test Pit	610629	6950730	9	3	0.1	2 Hours	4.2	340	0.40
LTTT08	Test Pit	618148	6944582	6.3	3.8	1.6	4 Hours	2.6	32	0.10
LTTT09	Test Pit	613967	6944956	7.2	3.8	1.8	2.5 Hours	1.9	0.9	0.15

Brine samples were obtained at the start and end of pumping of the test pits, while the trial trenches were sampled every day for field parameters of salinity, SG and pH, with samples retained for laboratory analysis on every second day.

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Brine grade variations during pumping show a muted response with most test pits moderately reducing in grade by less than 3%, while the grade increased by up to 10% at LTTT01. The full brine analysis results are provided in Appendix 1.

## Basal Aquifer

### Gravity Geophysical Survey

An initial ground gravity survey was completed in March 2020 (ASX announcement 7 May 2020) and followed up with an in-fill survey in July 2020 (ASX announcement 10 August 2020) for a total of approximately 200 line-kilometres with the aim of identifying drilling targets within the palaeovalley system as a first step of identifying a palaeochannel basal aquifer to target with future production bores.

The surveys comprised a total of 1,040 stations at approximate 200m spacing on traverses perpendicular to the inferred alignment of the palaeovalley. The gravity data was processed by gridding the Bouguer anomaly and regional separation from the Bouguer anomaly to produce a residual gravity anomaly that is considered to represent the broad palaeovalley geometry.

When compared to the known geology, the gravity highs are well correlated with mapped outcropping Paterson Formation and gravity lows are located within areas of low-lying regolith cover within the Throssell palaeovalley system, providing confidence in the regional model and general understanding of comparative palaeovalley in the region. Two gravity low anomalies have been found to be representative of deeply weathered bedrock instead of palaeovalley sediments. These are located in the central part of the tenement on the northern and southern side of the palaeovalley.

Following completion of the air-core program the gravity model has been updated by calibrating to the end-of-hole geology. The updated map of the residual gravity anomaly is presented in Figure 7.

The gravity model was used to generate drill targets for air-core drilling and inform the geological model away from areas of drilling control.

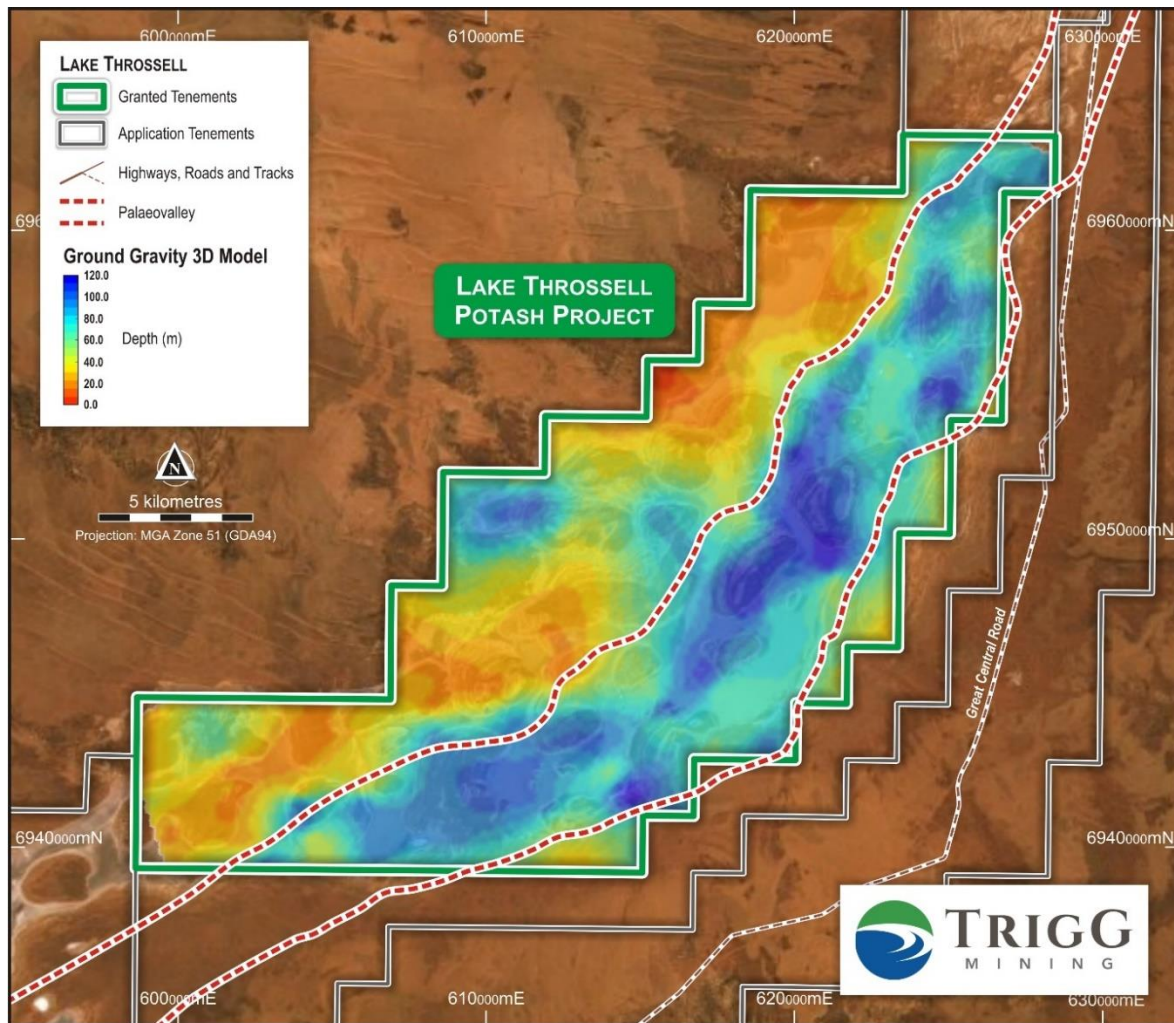


Figure 7: Gravity survey anomaly

### Air-core Drilling

The air-core drilling program commenced in late November 2020 to test aquifer targets at the base of the palaeovalley sequence determined from the gravity survey. The deepest sections of the palaeovalley are considered to be most prospective for sand and gravel aquifer sequences deposited in a palaeochannel environment.

The drill program was completed by a track-mounted air-core drill rig. The program commenced in November 2020 but was delayed due to wet weather in December 2020 with 16 holes completed, a further 38 drill holes were completed in February 2021 for a total of 5,623m (ASX announcements 21 December 2020 and 9 March 2021). The average hole depth was approximately 104m with a maximum depth of 144m (Figure 1 and Appendix 1).

The drill program confirmed the presence of a broad palaeovalley system approximately 100m deep with a thick lacustrine clay sequence and a number of deep aquifer targets of variable thickness and brine yielding. These included the basal sand and a glacial fluvial sand and gravel.

The basal sand is between approximately 5 to 17m thick and is typically a yellow, brown to green fine to medium grained sand with silty bands, typically located between 70 and 100m depth, and below the lacustrine clay on the eastern side of the palaeovalley associated with deposition in a medium to low energy palaeo-river system of likely Eocene to Pliocene age.

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The glacial fluvial sand and gravel is typically a light to dark grey fine to medium sand with rounded to sub-angular gravel and occasional silt, the gravel is broken by the drilling but can be assumed to potentially be up to cobble size. The thickness of this sequence may range from 1 to 2m up to 43m in the deepest section, estimated to be approximately 12m thick on average, and it is located mainly on the south and western sides of the palaeovalley. It is present as irregular zones either beneath the lacustrine clay or the fluvial basal sand or within zones of the Permian Saprolite zone, inferring that it is likely derived from a combination of an in-situ weathering profile of the coarse-grained Permian bedrock of fluvial glacial origin and a reworked pre-Eocene/Pliocene locally derived colluvial or alluvial deposit.

Drilling spoil samples were obtained for laboratory analysis of PSD to allow quantification of sand, silt, and clay portions from the various lithological zones across the system. Empirical equations have been applied to the PSD analysis which enables estimates of hydraulic conductivity and specific yield for the Mineral Resource Estimate. 62 samples in total were selected for laboratory analysis, which are discussed in the porosity and specific yield section below.

A total of 253 brine samples were submitted for assay, with results returning high grades of up to 5,800mg/L K (12.9kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>), with an average grade of 4,488mg/L K (10.0kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>). Of the 253 samples taken from the air-core program, 96% returned grades exceeding 5,000mg/L K confirming the extensive high-grade, low variability tenor of the brine within the Lake Throssell palaeovalley system.

### Geological Summary

A summary of the encountered geology of the project is presented in Table 2.

The geology is consistent with other lakes and palaeovalley sequences in the region. In the shallow sediments there is an evaporite surface, dominated by gypsum, underlain by more clayey dominated sequences with occasional thin granular and calcrete zones.

These superficial lithologies lie on top of a thick sequence of stiff lacustrine clay, which acts as a regionally confining aquitard with very low vertical hydraulic conductivity, meaning it hydraulically separates the shallow sediments of the palaeovalley from the basal aquifer sediments.

Beneath the lacustrine clay sequence is a fine to medium grained basal sand with silty and clayey bands of fluvial origin of between Eocene and Pliocene age. At the base of this fluvial system is the contact with the Permian age Paterson Formation, a palaeosurface that represents up to 200 million years of weathering, erosion and deposition. The contact is present in the base of the palaeovalley, and the Paterson Formation is a fluvial glacial deposit represented in fresh bedrock as dark to light grey poorly sorted siltstone, mudstone, sandstone and quartzite, with conglomerate beds.

The Paterson Formation is present and outcrops at the margins of the palaeovalley. Thick saprolite zones are present up to 50m in thickness along the palaeovalley margins, often dominated by silt and fine sand. Unconsolidated glacial fluvial sediments of mixed gravel and minor silt are present within this saprolite zone which are likely to be representative of either in-situ weathering or local colluvial deposits when at the contact with the overlying Cenozoic sediments. An example of the fluvial and glacial sequence is presented in Figure 8, where 43m of combined fluvial and glacial fluvial sediments are evident.

Permian Paterson Formation is outcropping on the western edge of the lake and between 3 and 5km to the southeast of the lake. A schematic cross-section of Lake Throssell is presented in Figure 9.



Figure 8: Chip trays showing the basal aquifer sequence (86 to 129m - gravel, fine sand, silt and minor clay)

### Hydrogeological Characteristics

The hydrogeology of a brine deposit is important to characterise as it is important to understand the groundwater flow regime and aquifer properties for the subsurface sediments in order to estimate future brine abstraction potential. At this early stage of the Lake Throssell Project, there has been no aquifer testing of the deep aquifer or modelling of the deposit, therefore the understanding of the system is mostly qualitative.

The water table at the lake surface is approximately 0.2 to 0.5m beneath the surface, it is considered to be relatively flat at the surface of the lake and is hypersaline. Within the islands the water table will likely rise reflecting the increase in topographic elevation. Outside of the lake area no drilling has been completed to estimate the depth to water table, however it is broadly assumed that the depth to water table will increase away from the lake surface as topography rises.

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Table 2: Current interpreted geological stratigraphy at Lake Throssell

Stratigraphic Layer	Assumed Age	Lithological Description	Range in Thickness	Aquifer Potential	Resource Domain
Lake Surface	Recent	Saturated Evaporitic sand and gravel in a silty matrix, gypsum up to 20mm in size.	4-6m	High	Surficial Aquifer
Alluvial Clay	Quaternary	Soft sandy brown clay with minor fine to medium grained sand, occasional evaporites.	5-25m	Low	
Lacustrine Clay	Neogene / Palaeogene	Stiff lacustrine clay with minor interbeds of fine sand and calcrete, present throughout the palaeovalley.	11-80m	Aquiclude, likely to provide leakage	Confining Layer
Fluvial Basal Sand	Pliocene/Eocene	Yellow to green fine to medium grained sand with intermixed clay and silt bands, mostly located on the eastern side of the palaeovalley.	2-17m	Moderate	Basal Aquifer
Glacial fluvial Sediments	Eocene to Permian	Sub-rounded to sub-angular mixed lithic gravel at base of palaeovalley fill sequence and within zones in the saprolite common throughout the southern and western part of the palaeovalley. Possibly weathered in-situ or re-worked in origin.	1-35m	Low to Major	
Saprolite	Permian	Light to dark grey to black, very fine to fine grained poorly sorted sand, silt, and clay.	3-50m	Low to Moderate	
Bedrock	Permian	Dark to light grey poorly sorted mudstone, siltstone, sandstone, conglomerate and tillite.	Unknown	Low	Bedrock (Resources not determined)

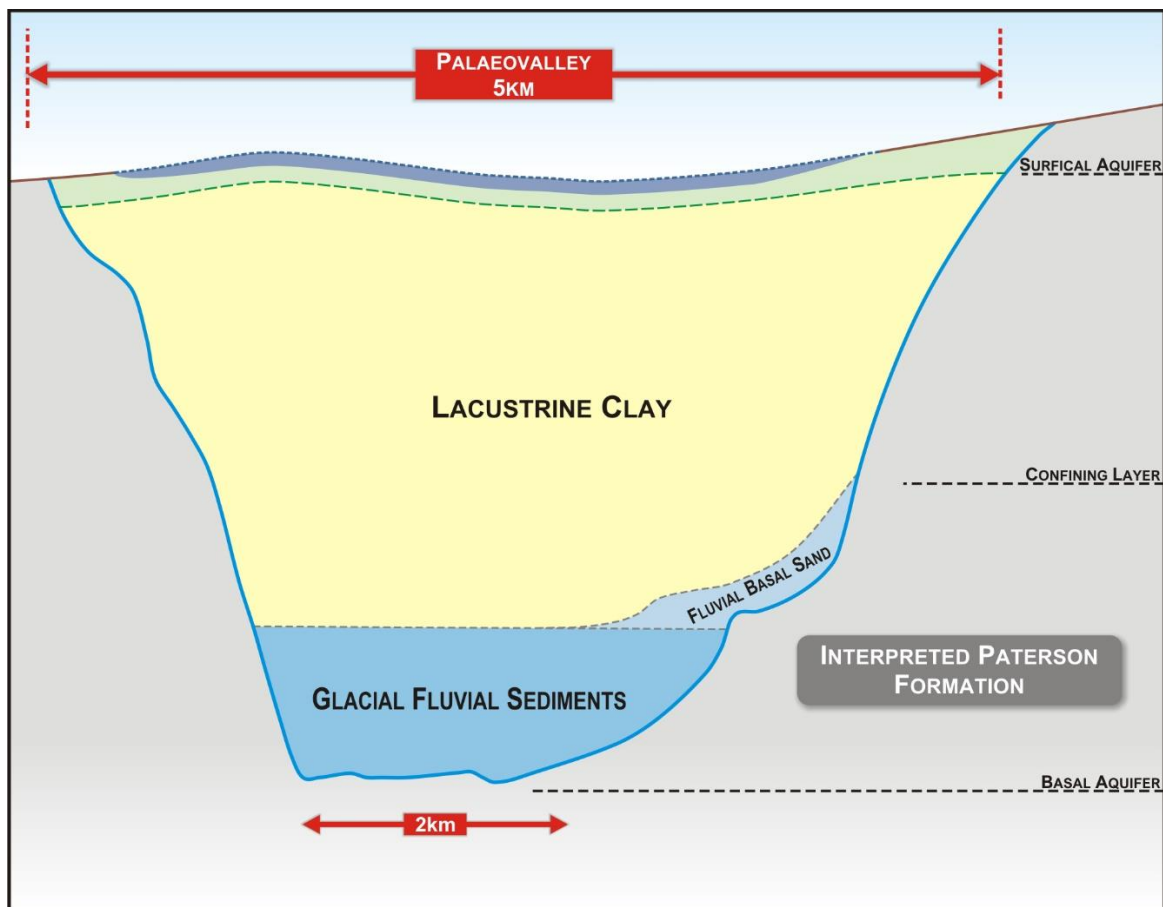


Figure 9: Schematic cross section of the palaeovalley sequence at Lake Throssell

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The salt lake acts as a point of discharge for the regional groundwater system. Groundwater flow in the shallow sediments within the lake’s catchment flows towards the lake surface where evaporation is dominant and there is a net loss to the system making the groundwater hypersaline in nature.

The aquifer potential of each of the stratigraphic layers is provided in Table 2 to provide an indication of potential for brine abstraction, test pumping of each of the aquifer zones is required to confirm their potential. The lake surface can be targeted in future by trenching, whilst production bore targets consist of the Eocene fluvial sediments, Permian glacial fluvial sediments and the saprolite.

In addition to specific yield (drainable porosity), which is discussed below in the context of the mineral resource estimate, hydraulic conductivity and specific storage are important hydrogeological aquifer properties to understand and measure for a brine deposit. Hydraulic conductivity is a measure of a material’s capacity to transmit water, the higher the value the more water can pass through. Aquifer’s generally have higher values of hydraulic conductivity than non-aquifers (otherwise known as aquitards and aquicludes). Values of hydraulic conductivity have been derived for the surficial aquifer from laboratory tests and test pumping analysis are presented in Table 3. The hydraulic conductivity of the other stratigraphic layers within the palaeovalley based on particle size distributions from drill core samples is provided in Table 4.

Specific storage is a confined aquifer property and is applicable to the basal aquifer which is likely to be confined. It is an aquifer property related to the pressure that the aquifer and brine are subject to at depth. Specific storage is not considered in this report and will be addressed when test production bores are installed and test pumped in the basal aquifer.

Table 3: Estimates of hydraulic conductivity for the surficial aquifer from test pumping

Location	Method	Hydraulic Conductivity (m/d)
LTTT01	Distance Drawdown analysis	7.8
LTTT01	Numerical Model Calibration	1.5
LTTT02	Distance Drawdown analysis	4.8
LTTT02	Numerical Model Calibration	0.5
LTTP01	Numerical Model Calibration	0.2
LTTP02	Numerical Model Calibration	0.8
LTTP03	Numerical Model Calibration	0.6
LTTP04	Numerical Model Calibration	1.9
LTTP05	Numerical Model Calibration	340
LTTP06	Numerical Model Calibration	32
LTTP07	Numerical Model Calibration	0.9

Table 4: Estimates of hydraulic conductivity from particle size distribution analysis

Stratigraphic Unit	Hydraulic Conductivity (m/d)		
	Min	Max	Geomean
Lacustrine Clay	0.01	0.61	0.09
Fluvial Basal Sand	0.35	1.12	0.75
Glacial Fluvial Sand and Gravel	0.07	4.36	0.37
Permian Saprolite	0.07	0.14	0.10

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### Brine Characteristics

The average potassium concentration from all samples within the surficial sediments is approximately 5,080mg/L K (11.3kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>), the lowest concentration is approximately 2,810mg/L K (6.3kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) at LGA26 (within an island) and the highest concentration is 6,660mg/L K (14.8kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) at LT016.

Higher concentrations of potassium appear to be located on the western side of the lake associated with accumulation of more evaporated brine. The lower concentrations of potassium are located in the northern side of the lake where it is likely more regular inflow of fresher surface water occurs. The potassium concentration distribution across the lake surface is presented in **Error! Reference source not found.**

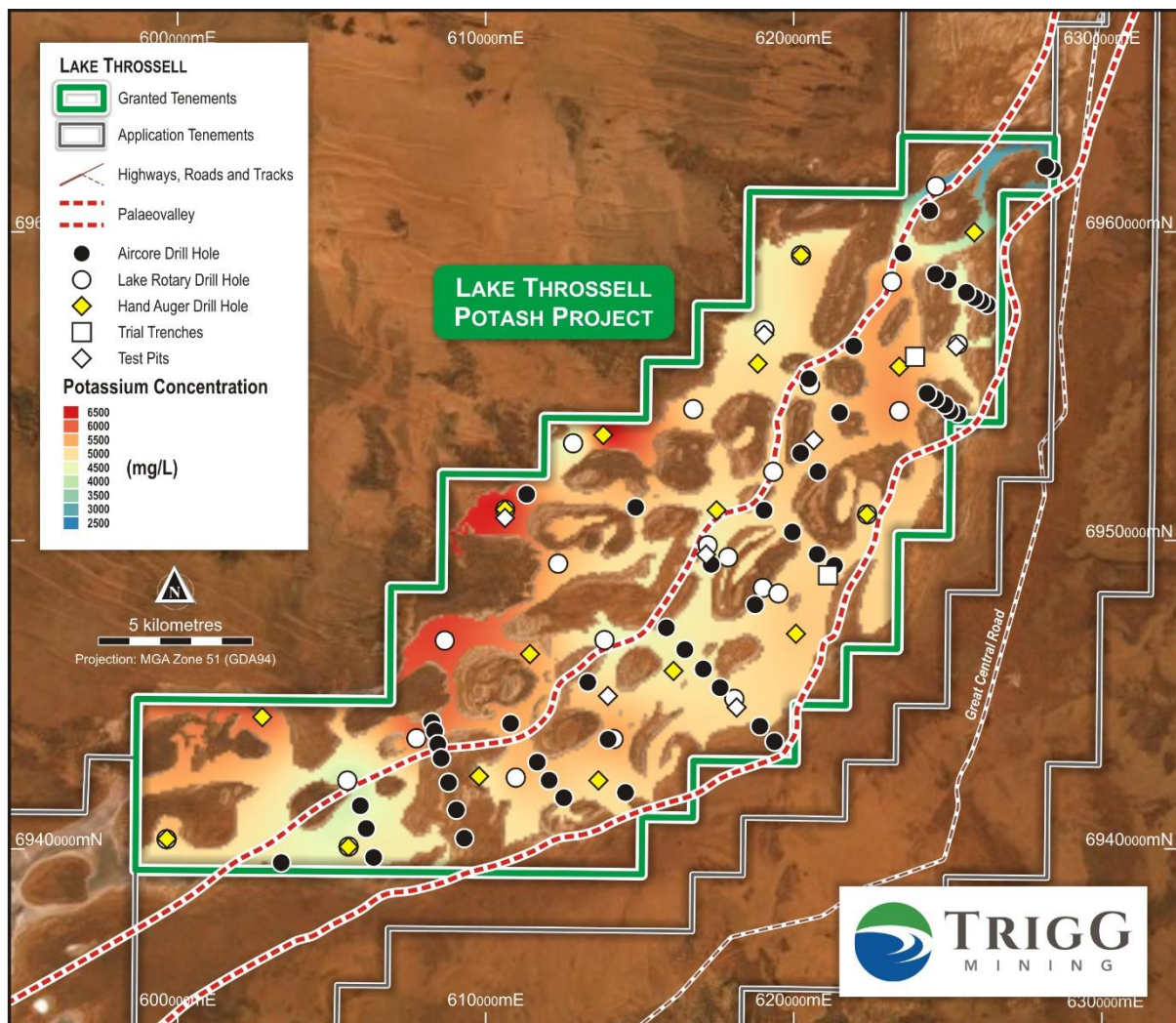


Figure 10: Potassium concentration at the lake surface

The average potassium concentration from samples within the deep palaeovalley is approximately 4,500mg/L K (10.0kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>), the lowest concentration is approximately 3,580mg/L K (8.0kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) at LTAC005 and the highest concentration is 5,500mg/L K (12.9kg/m<sup>3</sup> K<sub>2</sub>SO<sub>4</sub>) at LTAC040.

The potassium concentration and brine characteristics of the aquifers are very consistent across the palaeovalley. **Error! Reference source not found.** shows that the deep aquifer brine is somewhat uniform with concentration of between 4,000 and 5,000mg/L K and 8,000 and 10,000mg/L magnesium (Mg), in comparison to the lake sediments which has a wider distribution and is subject to more

environmental conditions such as recharge and evaporation has a more variable grade distribution. The end of pumping trench samples have been added to the distribution, which now form a cluster with slightly lower Mg and higher K concentrations compared to the deep aquifer samples.

Overall, the brine chemistry exhibits favourable characteristics for solar evaporative concentration and lower waste salts, with a relatively low Sodium to K ratio (16:1) and a high SO<sub>4</sub> concentration. The key average characteristics of the brine from the sampling to date at Lake Throssell are presented in Table 5.

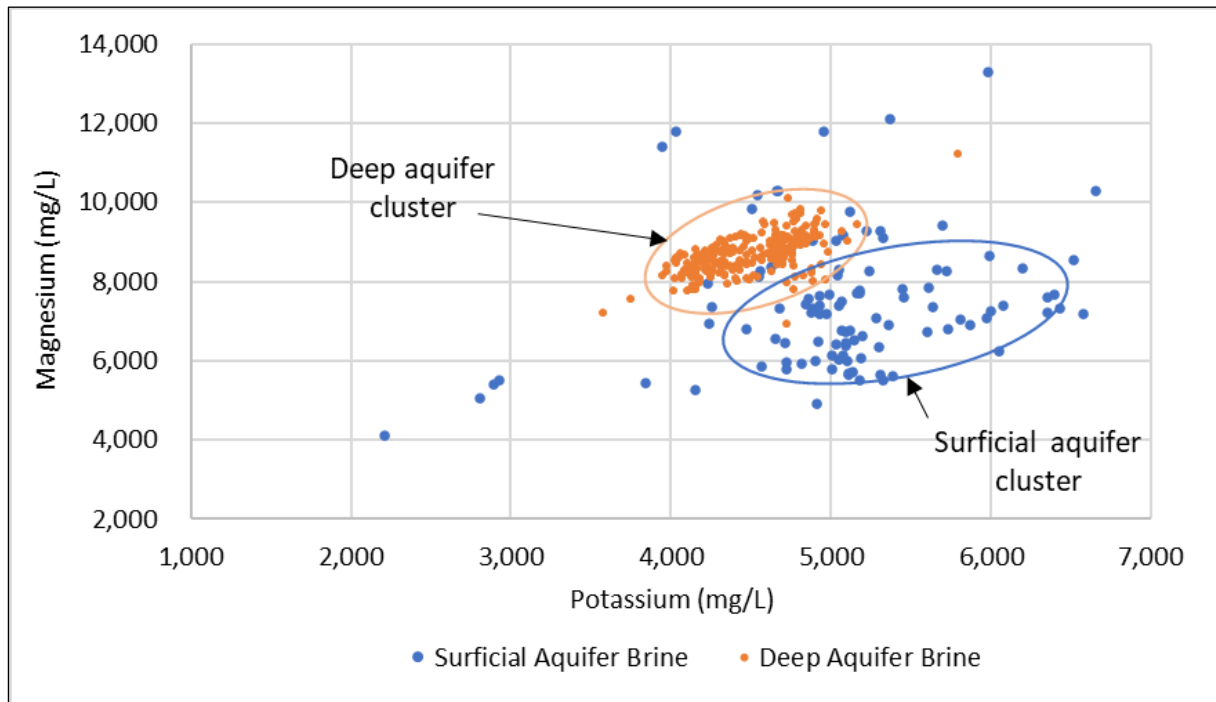


Figure 11: Potassium magnesium concentrations for the lake surface and deep brine aquifers

Table 5: Key average brine characteristics of Lake Throssell

Stratigraphy	K (mg/L)	SOP Equiv. (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Mg (mg/L)	Na (mg/L)	SO <sub>4</sub> (mg/L)	Total Dissolved Solids (mg/L)	K:Mg	Na:K
Surficial Aquifer	5,078	11.32	7,454	79,354	21,239	253,255	0.7	15.7
Basal Aquifer	4,498	10.03	8,682	76,755	24,141	255,365	0.5	17.6

Note: All concentrations based on average of all samples obtained to date and not spatially weighted. SOP equivalent or K<sub>2</sub>SO<sub>4</sub> is calculated from K x 2.23.

### Porosity and Specific Yield

The total volume of brine in a brine deposit is determined by the total porosity, whilst porosity is made up of specific retention (also known as retained porosity) and specific yield (also known as effective porosity). Specific yield is the percent volume of water that can be drained by gravity from a saturated volume of sediment. While specific retention is the percent volume that is retained under gravity drainage. The specific yield is the ratio used to define the drainable volume of a brine deposit. Portions of specific retention in the lake surface are accessible in addition to the specific yield but require additional modifying factors around lake recharge effects to be determined before quantification.

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Total porosity and specific yield have been measured in the laboratory from core plugs obtained from the Lexan tubes during the heli-rotary auger program and using empirical equations from the PSD results obtained during the air-core program.

Core plugs of the lake surface sediments were taken at Corelabs, Perth and analysed using the saturated centrifuge method.

Specific yield has also been determined from test pumping of the lake surface from trial trenches and test pits. These tests sample a much larger zone of the sequence and provide a bulk estimate of Sy over the saturated thickness of the excavation.

The results indicate that the sequence is highly heterogeneous throughout the profile with an average total porosity of 0.38 and the average and weighted average specific yield of 0.17. Results are presented in Table 6.

Table 6: Total porosity and specific yield estimates for the lake surface

Hole ID	Sample Depth (m)	Sample Interval (m)	Total Porosity (-)	Specific Yield (-)
LTAG01	1.8	0.1	0.34	0.24
LTAG01	3.3	0.1	0.36	0.19
LTAG06	2.5	0.1	0.35	0.17
LTAG06	4	0.1	0.36	0.17
LTAG06	4.8	0.1	0.36	0.17
LTAG14	2.5	0.1	0.36	0.16
LTAG14	1.8	0.1	0.26	0.10
LTAG14	3.3	0.1	0.30	0.11
LTAG14	6.3	0.1	0.35	0.23
LTAG20	2.5	0.1	0.49	0.22
LTAG20	1.8	0.1	0.39	0.16
LTAG20	4	0.1	0.36	0.17
LTAG20	5.5	0.1	0.40	0.19
LTAG24	5.5	0.1	0.31	0.16
LTAG26	2.5	0.1	0.49	0.20
LTAG26	1.8	0.1	0.45	0.13
LTAG26	4	0.1	0.47	0.18
LTAG26	5.5	0.1	0.46	0.17
LTTT01	0.3 to 4.5	4.2	n/a	0.40
LTTT02	0.3 to 4.5	4.2	n/a	0.40
LTTT01	0.3 to 3.7	3.4	n/a	0.01
LTTT02	0.3 to 3	2.7	n/a	0.02
LTTT03	0.3 to 4	3.7	n/a	0.01
LTTT04	0.3 to 3	2.7	n/a	0.05
LTTT05	0.3 to 3	2.7	n/a	0.40
LTTT06	0.3 to 3.8	3.5	n/a	0.10
LTTT07	0.3 to 3.8	3.5	n/a	0.15
		Minimum	0.26	0.01
		Maximum	0.49	0.40
		Average	0.38	0.17
		Weighted Average*	N/A	0.17

\*Removed the upper and lower outliers (LTTT02 and LTTT03) in the trench pumping to account for high heterogeneity.

During the air-core program soil samples were obtained for laboratory analysis of PSD to allow quantification of sand, silt and clay portions from the various lithological zones across the system. A field capacity regression calculation at 33kPa (Saxton Rawls 2006) has been used to determine specific yield (effective porosity).

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A total of 62 samples were selected for laboratory analysis mostly targeting the potentially more productive aquifer sequences of sand sequences in the glacial fluvial sediments to provide a better understanding of the lithological composition relative to the geological logging. The samples were grab samples from drilling spoil and represent a 3m composite interval.

The analysis results demonstrate good correlation of aquifer properties to lithological description and are considered reasonable for disturbed sample analysis, the results are presented in Table 7 below. The exception being the Lacustrine Clay samples which shows some bias to more granular lithologies than a pure clay.

Table 7: Total porosity and specific yield estimates from particle size distribution analysis

Stratigraphic Unit	Number of Samples	Specific Yield (-)		
		Min	Max	Geomean
Lacustrine Clay	4	0.03	0.19	0.09
Fluvial Basal Sand	6	0.17	0.26	0.23
Glacial Fluvial Sand and Gravel	48	0.10	0.32	0.18
Permian Saprolite	4	0.09	0.12	0.10

### Mineral Resource Estimation Methodology

The MRE is constrained by the available data, geological confidence, drilling density, sampling intervals and tenement boundaries. This MRE covers the following updates:

- The existing geology and block models have been updated with the trench geology and end of test pumping brine samples
- The resource domains have been simplified by grouping the target aquifers together into an upper Surficial Aquifer, a Confining Layer and a lower Basal Aquifer
- New Indicated Mineral Resources have been estimated for the Surficial Aquifer
- Inferred Mineral Resources have been updated for all other Resource domains, and
- No Measured Mineral Resources or Ore Reserves have been estimated.

The geology model was constructed in Leapfrog Geo v6 implicit modelling software. The model used all available drilling data, surface mapping and geophysical data to model the geology across Lake Throssell and the Palaeovalley sequence. The topography of the model was derived from 1 second Shuttle Radar Tomography Mission (SRTM) derived hydrological digital elevation model. All drill holes were levelled to this topography in the model.

All brine assays (355) for potassium, sulphate and magnesium were brought into the model as intervals where taken from drilling, rotary auger, hand-auger and test pumping.

The Edge module in Leapfrog Geo v6 was used for numerical estimation and block modelling. The variography of the deposit was modelled using the major axis and radial plot for guidance. Estimators were set up for potassium, sulphate and magnesium for the below water table domain. The domain was clipped to boundaries of the tenements and the island perimeters (lake surface only) as hard boundaries. The base of the domain was defined as 226m Australian Height Datum (AHD). Standard parent block sizes of 1,000m in the x and y direction and 10m in the z direction were used. Sub blocking was used to refine the block model in areas where geological surfaces intersect blocks. Parent blocks were split by automated sub-blocking by up to two sub-blocks in the x and y direction. Parameter concentrations were estimated across the blocks using Ordinary Kriging, ellipsoid search parameters were assigned following review of the variography of each parameter.

The search parameters for the block model are listed below:

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## Lake Throssell Potash Project

July 2021 Resource Estimate Reported in Accordance with JORC Code 2012

Ellipsoid Ranges - Max. = 4500m, Int. = 2,900m, Min. = 185m

No. of Samples – Max = 20, Min = 1.

The block model grade distributions are presented in **Error! Reference source not found.** to **Error! Reference source not found.** with cross sections presented in Figure 14 to Figure 17.

An inverse distance squared (ID2) estimator was run for potassium to check the accuracy of the calculation. The average grade of each model swath (average cell value in one plane) and the plots of each model have been reviewed. These plots show that the model adopted is appropriate when plotted against the ID2 method and assayed values.

Specific yield for the lake surface was estimated from the weighted average of the core analysis and trench pumping analysis. For all other stratigraphy's PSD analysis of disturbed lithological samples using field capacity regression calculations at 33kPa (Saxton Rawls 2006) and comparisons to publicly available data from similar geological settings. The adopted specific yield and total porosity for each stratigraphy of the model is presented in Table 8 and Table 9.

SOP grade from potassium concentrations were calculated using a conversion of 2.23, accounting for the atomic weight of sulphate (sulphur and oxygen) in the  $K_2SO_4$  formula.

Resource tonnages were calculated by multiplying the volume of the block model in each lithology by the specific yield and SOP grade to obtain the drainable SOP volume.

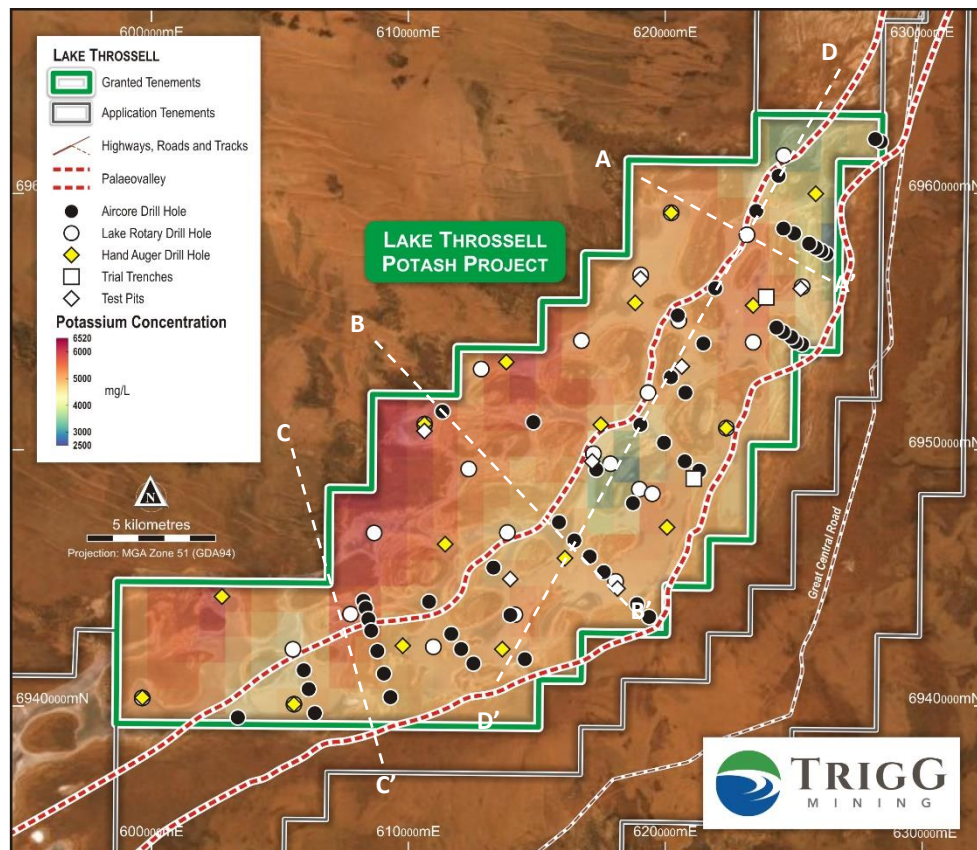


Figure 12: Lake Throssell shallow potassium grade distribution and sample points (370mRL depth slice)

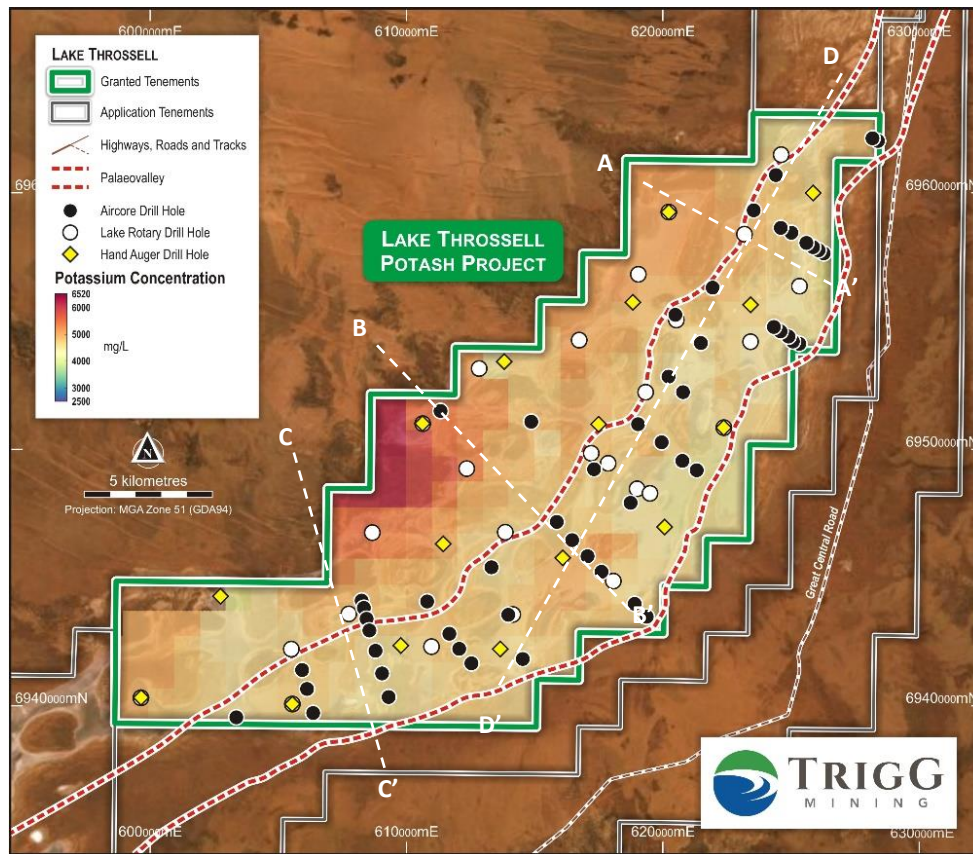


Figure 13: Lake Throssell deep potassium grade distribution and sample points (280mRL depth slice)

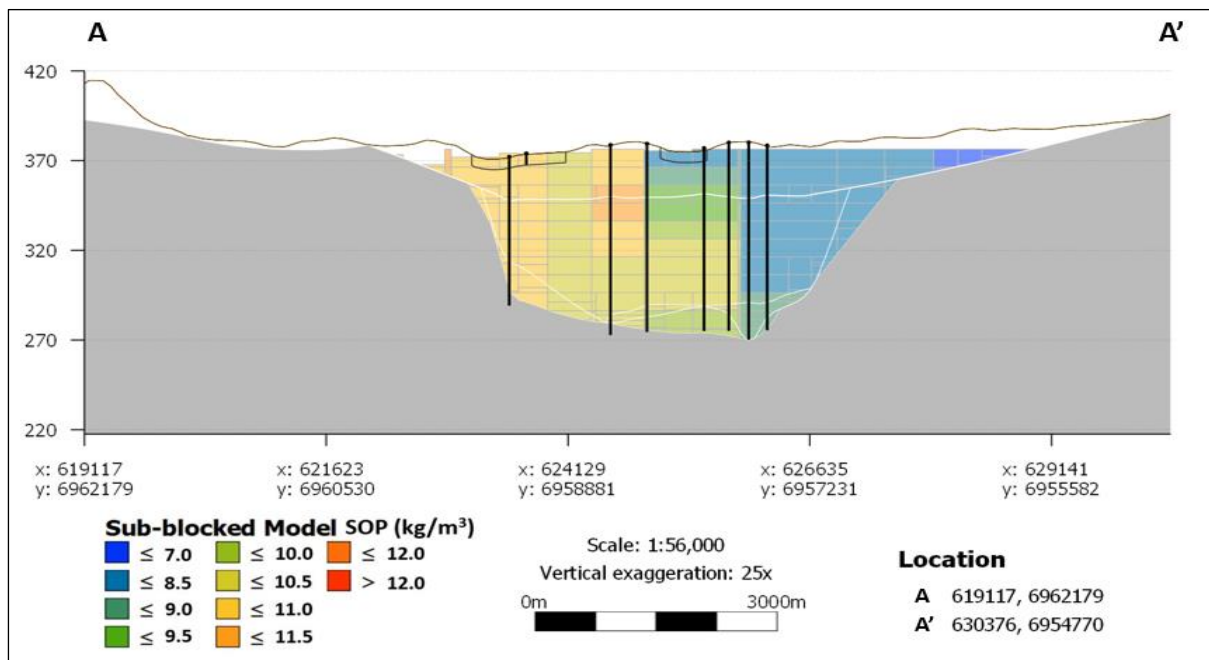


Figure 14: Block model cross section A-A'

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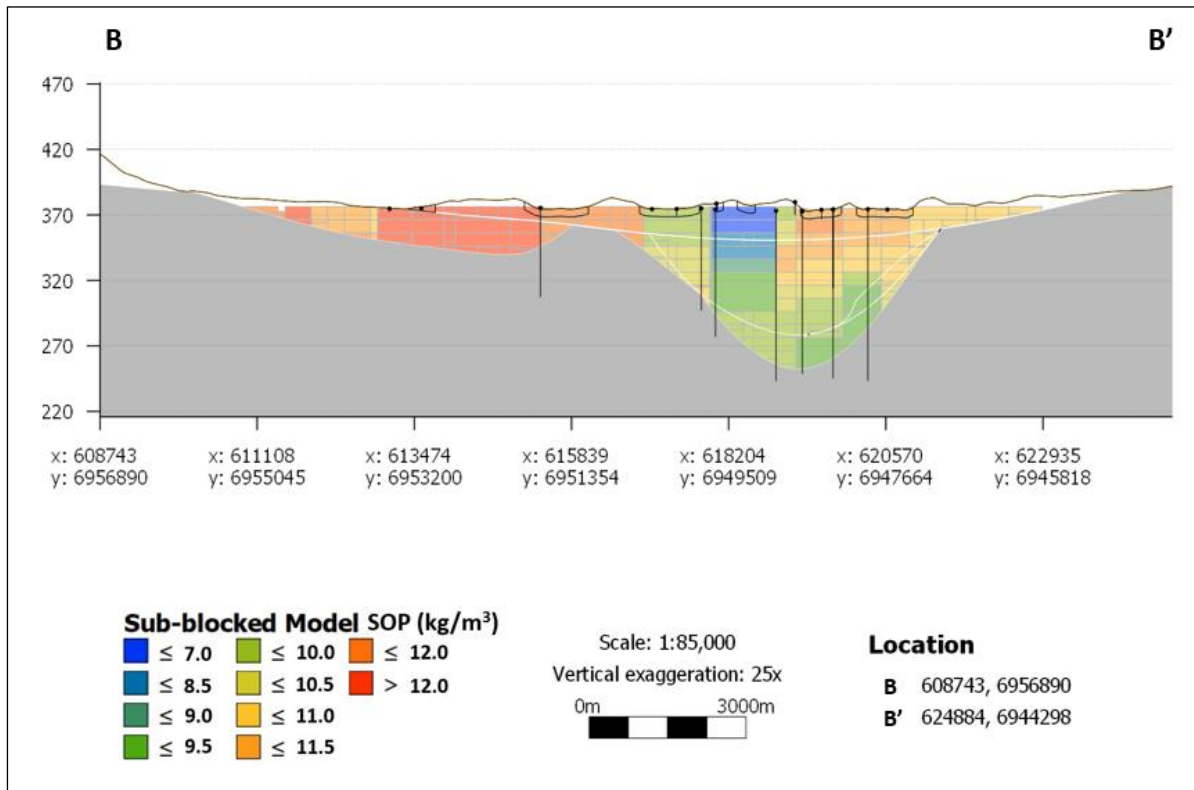


Figure 15: Block model cross section B-B'

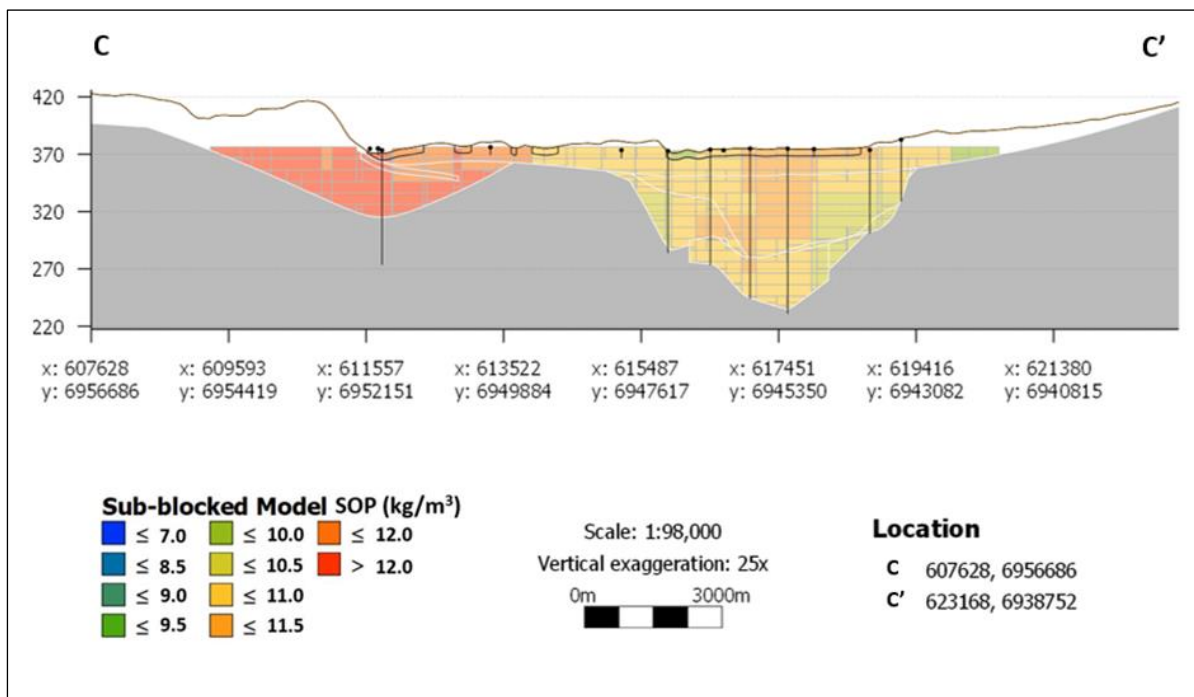


Figure 16: Block model cross section C-C'

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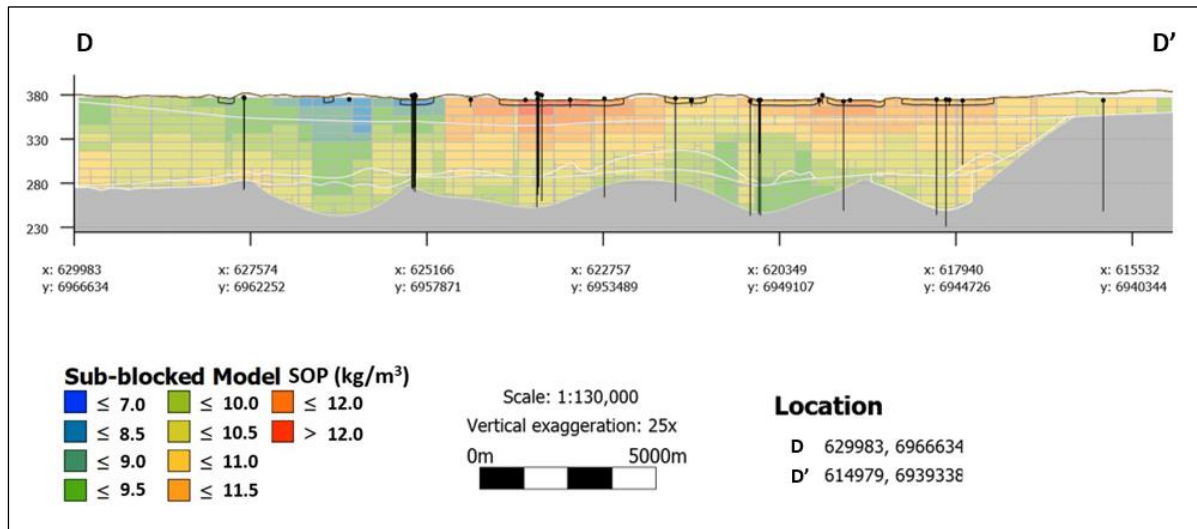


Figure 17: Block model long section D-D'

The Indicated Mineral Resource has been calculated based on the following:

- Drilling and testing has confirmed local site geology and aquifer geometry
- Aquifer hydraulic properties (hydraulic conductivity and specific yield) have been determined by two independent methods
- Test pumping has been completed to demonstrate extractability
- A number of brine samples have been collected from a selection of locations to confirm brine concentrations, and
- These conditions are only met for the top six metres of the lake surface of the surficial aquifer.

The Inferred Mineral Resource has been calculated based on the following:

- Geological evidence exists to imply but not verify the existence of brine grade and aquifer geometry for the entire deposit due to some wide drill and sample spacing
- Proven geophysical techniques have been used to infer palaeovalley extents away from the main drilling areas and extend the estimate into the pending tenements, and
- Aquifer properties can be calculated from limited laboratory tests, PSD and other publicly available data in comparative geological settings.

Total porosity and total brine SOP mass is provided to compare the total SOP tonnes with the drainable Resources. As can be seen, the total brine volume is significantly higher than reporting drainable brine volumes. The drainable brine volume represents the amount of SOP that can be abstracted from the deposit which is dependent on underlying porosity, permeability and specific yield of the deposit. For economic production, the drainable brine volume is the most important volume because only a proportion of brine present can be typically abstracted from the deposit.

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## Lake Throssell Potash Project

Lake Throssell July 2021 Resource Estimate Reported in Accordance with JORC Code 2012

Table 8: Lake Throssell Indicated Mineral Resource Estimate

Resource Domain	Volume (10 <sup>6</sup> m <sup>3</sup> )	Total Porosity (-)	Brine Volume (10 <sup>6</sup> m <sup>3</sup> )	Specific Yield (-)	Drainable Brine Volume (10 <sup>6</sup> m <sup>3</sup> )	K Grade (mg/L)	K Mass (Mt)	SO <sub>4</sub> Grade (mg/L)	SO <sub>4</sub> Mass (Mt)	Mg Grade (mg/L)	Mg Mass (Mt)	Equivalent SOP Grade (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Drainable Brine SOP Mass (Mt)	Total Brine SOP Mass (Mt)
Surficial Aquifer	1,008	0.40	403	0.17	170	4,985	0.8	22,125	3.8	7,764	1.32	11.1	1.9	4.5
Total Indicated Resources	1,008	0.40	403	0.17	170	4,985	0.8	22,125	3.8	7,765	1.32	11.1	1.9	4.5

Note: Errors may be present due to rounding

Table 9: Lake Throssell Inferred Mineral Resource Estimate

Resource Domain	Volume (10 <sup>6</sup> m <sup>3</sup> )	Total Porosity (%)	Brine Volume (10 <sup>6</sup> m <sup>3</sup> )	Specific Yield (%)	Drainable Brine Volume (10 <sup>6</sup> m <sup>3</sup> )	K Grade (mg/L)	K Mass (Mt)	SO <sub>4</sub> Grade (mg/L)	SO <sub>4</sub> Mass (Mt)	Mg Grade (mg/L)	Mg Mass (Mt)	Equivalent SOP Grade (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Drainable Brine SOP Mass (Mt)	Total Brine SOP Mass (Mt)
Surficial Aquifer	3,074	0.43	1,313	0.10	310	4,605	1.4	21,910	6.8	7,820	2.4	10.3	3.2	13.5
Confining Layer	8,793	0.45	3,957	0.04	350	4,595	1.6	23,140	8.1	8,240	2.9	10.3	3.6	40.6
Basal Aquifer	4,446	0.37	1,659	0.12	545	4,640	2.5	23,350	12.7	8,320	4.5	10.3	5.6	17.2
Total Inferred Resource	16,313		6,929		1,205	4,620	5.6	22,920	27.6	8,170	9.8	10.3	12.4	71.2

Note: Errors may be present due to rounding, approximately 2.90Mt of Drainable SOP Mass is present in Exploration Licence Applications E38/3544, E38/3483, E38/3458, and E38/3537.

## Exploration Target

The Exploration Target is an estimate of the exploration potential of a mineral deposit is presented in Table 10. In a brine hosted deposit, the Exploration Target determines a lower and upper estimate by varying the geological extent, drainable porosity, and brine grade within reasonable bounds based upon the information available.

The geological extent (area and thickness) is determined from a combination of the modelled geological, the gravity model, the mapped outcropping geology and the conceptual model of regionally described palaeovalley systems.

Islands on the lake surface have been removed from the lake surface and alluvial clay sediment volume calculation. Brine grade range is based on the average brine grades from the Resource Tables, with the upper and lower estimates factored for the pending tenements where no data is presently available.

The Exploration Target encompasses the granted tenement E38/3065 and the surrounding pending tenements currently under application. There has been no work completed on the pending tenements meaning that all estimates are based upon reasonable extrapolation from the work completed on E38/3065. At the time of reporting Trigg sees no reason why these tenements will not be granted in the future.

Table 10: Lake Throssell Exploration Target

Resource Domain	Thickness (m)	Area (km <sup>2</sup> )	Sediment Volume (10 <sup>6</sup> m <sup>3</sup> )	Specific Yield (-)	Drainable Brine (10 <sup>6</sup> m <sup>3</sup> )	K Grade (mg/L)	K Mass (Mt)	Equiv. SOP Grade (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Drainable Brine SOP Mass (Mt)
Surficial Aquifer	19	70	656	0.09	61	3,739	0.2	8.3	0.5
Confining Layer	60	68	4,050	0.03	122	4,356	0.5	9.7	1.2
Basal Aquifer	20	144	1,101	0.10	106	3,961	0.4	8.8	0.9
Total Lower Estimate		282	5,807		288	4,081	1.2	9.1	2.6
Surficial Aquifer	26	88	1,156	0.12	134	4,526	0.6	10.1	1.4
Confining Layer	70	90	6,300	0.05	315	4,740	1.5	10.6	3.3
Basal Aquifer	35	269	3,469	0.14	496	4,277	2.1	9.5	4.7
Total Upper Estimate		447	10,925		945	4,466	4.2	10.0	9.4

Note: Errors may be present due to rounding, approximately 2.45 Mt in the lower estimate and 8.76 Mt in the upper estimate of equivalent SOP is present in Exploration Licence Applications E38/3544, E38/3483, E38/3458 and E38/3537. SOP is calculated by multiplying potassium by 2.23.

The potential quantity and grade of the Exploration Target is conceptual in nature. There has been insufficient exploration in these areas to estimate a Mineral Resource. It is uncertain if further exploration will result in the estimation of a Mineral Resource.

## APPENDIX 1 – Drill hole and brine analysis tables

Lake Throssell hand auger collar location and assay result

Site ID	Easting	Northing	Hole depth (m)	K (mg/L)	SOP Equiv. <sup>1</sup> (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Mg (mg/L)	Na (mg/L)	SO <sub>4</sub> (mg/L)	TDS (mg/L)
LT001	625,864	6959997	1.20	3,840	8.56	5,440	57,600	13,700	187,000
LT002	620,233	6959250	1.10	5,120	11.42	9,750	85,800	25,000	284,000
LT003	618832	6955734	1.20	5,090	11.35	6,740	75,900	20,600	237,000
LT004	623424	6955635	1.20	5,610	12.51	7,830	88,500	20,900	276,000
LT005	622383	6950849	1.10	5,150	11.48	6,510	82,700	18,000	256,000
LT006	617496	6950979	1.20	4,910	10.95	4,920	69,900	15,300	220,000
LT007	610629	6951011	1.10	6,580	14.67	7,180	81,000	23,900	259,000
LT008	620071	6946977	1.20	5,240	11.69	8,250	89,100	20,300	280,000
LT009	616099	6945768	1.20	4,820	10.75	5,910	78,200	18,800	235,000
LT010	611438	6946320	1.20	5,600	12.49	6,740	89,500	20,300	272,000
LT011	613656	6942220	1.20	5,040	11.24	8,170	84,900	21,700	269,000
LT012	609780	6942352	1.10	4,840	10.79	7,420	84,400	23,000	263,000
LT013	605549	6940072	1.20	4,880	10.88	7,220	72,100	20,500	231,000
LT014	599651	6940332	1.00	5,370	11.98	12,100	92,900	30,300	317,000
LT015	602745	6944274	1.10	5,980	13.34	13,300	91,900	32,400	322,000
LT016	613817	6953422	0.80	6,660	14.85	10,300	92,100	28,200	308,000

Lake Throssell heli-rotary auger location and assay results

Site ID	Easting	Northing	Sample depth (m)	K (mg/L)	SOP equiv. <sup>1</sup> (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Mg (mg/L)	Na (mg/L)	SO <sub>4</sub> (mg/L)	TDS (mg/L)
LTAG01	623221	6954229	0	5,720	12.76	8,260	93,300	21,800	284,000
			2.5	5,460	12.18	7,600	82,600	20,100	269,000
LTAG02	625430	6956409	0	4,670	10.41	8,730	84,300	19,700	270,000
			0.5	4,750	10.59	8,810	84,000	20,300	267,000
			2.5	4,630	10.32	8,380	80,400	19,800	253,000
			4	4,550	10.15	8,140	78,700	19,200	256,000
			5.5	4,560	10.17	8,280	79,700	19,300	250,000
LTAG03	619489	6948228	0	5,180	11.55	7,720	84,400	21,200	270,000
			2.5	5,450	12.15	7,800	89,800	21,600	284,000
			4	5,660	12.62	8,310	92,100	22,300	290,000
LTAG06	617249	649900	0	4,720	10.53	5,950	76,900	17,800	230,000
			1	4,720	10.53	5,780	75,300	17,700	230,000
			2.5	4,570	10.19	5,840	73,400	17,100	225,000
LTAG07	618264	6944914	0	5,050	11.26	8,310	83,100	20,200	265,000

<sup>1</sup> SOP equivalent (K<sub>2</sub>SO<sub>4</sub>) is calculated by multiplying potassium by 2.23.

Site ID	Easting	Northing	Sample depth (m)	K (mg/L)	SOP equiv. <sup>1</sup> (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Mg (mg/L)	Na (mg/L)	SO <sub>4</sub> (mg/L)	TDS (mg/L)
			1	5,070	11.31	7,510	83,100	21,000	266,000
			2.5	5,180	11.55	7,790	86,600	21,300	268,000
			4	5,160	11.51	7,690	85,500	20,600	264,000
			5.5	4,930	10.99	7,390	79,700	20,000	263,000
LTAG08	613965	6946765	0	4,510	10.06	9,850	96,600	24,500	301,000
			1	4,670	10.41	10,300	97,900	24,900	299,000
			2.5	4,540	10.12	10,200	95,000	24,800	300,000
			4	4,660	10.39	10,300	96,900	25,700	305,000
LTAG09	614144	6943570	1	5,640	12.58	7,360	90,100	20,800	278,000
			2.5	4,930	10.99	7,170	80,100	18,800	285,000
			4	5,990	13.36	8,640	94,700	23,200	290,000
LTAG10	610882	6942305	1	5,360	11.95	6,920	83,400	22,700	259,000
			2.5	5,050	11.26	6,040	80,500	21,400	244,000
			4	4,900	10.93	5,980	79,100	21,500	244,000
LTAG11	603216	6942167	0	4,030	8.99	11,800	88,900	27,500	283,000
			1	3,950	8.81	11,400	83,200	25,400	285,000
LTAG12	605545	6940077	0	4,470	9.97	6,790	66,500	19,900	234,000
			1	4,680	10.44	7,320	71,400	20,700	236,000
			2.5	4,890	10.90	7,330	73,700	22,000	230,000
LTAG13	599494	6940005	0	4,960	11.06	11,800	91,500	31,800	311,000
LTAG14	607702	6943633	0	5,970	13.31	7,070	82,600	23,000	265,000
			1	6,000	13.38	7,240	85,300	23,600	266,000
			2.5	6,080	13.56	7,390	85,100	23,500	274,000
			5.5	5,810	12.96	7,060	81,700	23,000	267,000
LTAG15	608710	6946765	0	6,200	13.83	8,330	92,500	23,800	314,000
			1	6,520	14.54	8,560	98,100	26,000	308,000
			4	6,050	13.49	6,240	82,300	21,600	257,000
LTAG16	612341	6949239	0	5,390	12.02	5,600	75,000	18,400	232,000
			2.5	5,330	11.89	5,520	75,500	18,300	231,000
LTAG17	610629	6951013	0	6,350	14.16	7,220	79,900	25,100	261,000
			1	6,430	14.34	7,310	81,900	25,200	252,000
			4	6,350	14.16	7,590	81,900	25,500	265,000
			5.5	6,400	14.27	7,670	83,300	26,000	263,000
LTAG18	612830	6953124	0	4,240	9.46	6,930	55,800	21,700	184,000
			1	4,260	9.50	7,370	56,700	21,100	193,000
LTAG19	616742	6954229	0	5,110	11.40	5,660	70,200	18,500	221,000
			1	5,180	11.55	5,500	71,900	18,400	217,000
			2.5	5,110	11.40	5,690	68,400	18,500	220,000
LTAG20	619339	6952229	0	5,280	11.77	7,070	89,400	20,900	259,000
			1	5,120	11.42	6,750	85,400	19,800	262,000

Site ID	Easting	Northing	Sample depth (m)	K (mg/L)	SOP equiv. <sup>1</sup> (K <sub>2</sub> SO <sub>4</sub> ) (kg/m <sup>3</sup> )	Mg (mg/L)	Na (mg/L)	SO <sub>4</sub> (mg/L)	TDS (mg/L)
			2.5	5,090	11.35	6,390	84,900	19,800	264,000
			4	5,200	11.60	6,620	86,400	20,300	266,000
LTAG21	622383	6950850	0	5,090	11.35	6,450	79,000	19,900	253,000
			1	5,010	11.17	6,150	80,500	19,400	247,000
LTAG22	620534	6955035	0	5,080	11.33	6,120	76,100	18,700	234,000
			3.25	5,010	11.17	5,800	76,200	18,500	231,000
			4	5,100	11.37	6,000	78,600	18,600	233,000
			5.5	5,190	11.57	6,070	77,600	18,700	235,000
			7	5,140	11.46	5,700	73,300	18,100	237,000
			8.5	5,310	11.84	5,640	74,900	18,300	237,000
LTAG23	619041	6956827	0	4,710	10.50	6,450	66,700	20,800	218,000
			1	4,650	10.37	6,550	67,900	21,000	216,000
			4	5,050	11.26	7,400	74,000	23,600	235,000
			5.5	4,990	11.13	7,660	72,400	24,100	237,000
LTAG24	620233	6959251	0	4,890	10.90	9,020	79,900	25,600	280,000
			1	5,080	11.33	9,190	83,900	26,300	274,000
			2.5	5,220	11.64	9,290	81,800	26,300	276,000
			4	5,310	11.84	9,270	84,800	27,400	280,000
LTAG25	623191	6958379	0	5,730	12.78	6,790	82,400	20,900	260,000
			1	5,300	11.82	6,330	76,400	19,700	257,000
LTAG26	624624	6961485	2.5	2,810	6.27	5,040	38,100	13,200	127,000
			4	2,890	6.44	5,400	38,800	14,400	130,000
			5.5	2,930	6.53	5,510	39,000	14,500	136,000

Lake Throssell air-core drill hole locations

Collar ID	Easting (GDA94 Z51)	Northing (GDA94 Z51)	Azimuth	Dip	RL (mAHD)	Depth (m)
LTAC001	628388	6962021	0	-90	372	105
LTAC002	628176	6962125	0	-90	372	102
LTAC003	625859	6957880	0	-90	383	105
LTAC004	626076	6957761	0	-90	387	110
LTAC005	626271	6957639	0	-90	380	103
LTAC006	625599	6958044	0	-90	375	102
LTAC007	625013	6958442	0	-90	374	105
LTAC008	625073	6954204	0	-90	380	120
LTAC009	624590	6954598	0	-90	370	109
LTAC010	624330	6954770	0	-90	381	129
LTAC011	624900	6954397	0	-90	344	105
LTAC012	625321	6954113	0	-90	378	120
LTAC013	626684	6957399	0	-90	376	87
LTAC014	624598	6958634	0	-90	374	106
LTAC015	619031	6950979	0	-90	370	97
LTAC016	619951	6950276	0	-90	369	130

Collar ID	Easting (GDA94 Z51)	Northing (GDA94 Z51)	Azimuth	Dip	RL (mAHD)	Depth (m)
LTAC017	620753	6949534	0	-90	368	60
LTAC018	620767	6949553	0	-90	367	129
LTAC019	621325	6949188	0	-90	372	131
LTAC020	618904	6943976	0	-90	376	73
LTAC021	619372	6943476	0	-90	372	54
LTAC022	614538	6941828	0	-90	372	126
LTAC023	609051	6941266	0	-90	379	108
LTAC024	608793	6942149	0	-90	377	108
LTAC025	605931	6941400	0	-90	370	106
LTAC026	606360	6939722	0	-90	371	108
LTAC027	606125	6940664	0	-90	374	104
LTAC028	603361	6939557	0	-90	381	105
LTAC029	608342	6943819	0	-90	374	100
LTAC030	608554	6942945	0	-90	378	104
LTAC031	609306	6940345	0	-90	383	107
LTAC032	608445	6943398	0	-90	372	102
LTAC033	608235	6944107	0	-90	370	95
LTAC034	612058	6942224	0	-90	366	105
LTAC035	612537	6941660	0	-90	381	106
LTAC036	611676	6942812	0	-90	376	111
LTAC037	610808	6944073	0	-90	375	101
LTAC038	613975	6943553	0	-90	378	129
LTAC039	613316	6945407	0	-90	364	62
LTAC040	617061	6945835	0	-90	365	131
LTAC041	615865	6947171	0	-90	372	89
LTAC042	616463	6946466	0	-90	373	101
LTAC043	617612	6945228	0	-90	374	144
LTAC044	618747	6947918	0	-90	372	124
LTAC045	617320	6949225	0	-90	367	78
LTAC046	614871	6951078	0	-90	371	68
LTAC047	611333	6951499	0	-90	351	100
LTAC048	620788	6952231	0	-90	372	117
LTAC049	620226	6952834	0	-90	377	128
LTAC050	621488	6954148	0	-90	375	112
LTAC051	620493	6955247	0	-90	374	68
LTAC052	621948	6956306	0	-90	371	99
LTAC053	623545	6959320	0	-90	378	83
LTAC054	624413	6960692	0	-90	378	106

Lake Throssell air-core assay results

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC001	102	102	570	4,420	9,848	9.85	77,000	8,000	7,470	22,400	248,000

<sup>2</sup> SOP equivalent (K<sub>2</sub>SO<sub>4</sub>) is calculated by multiplying potassium by 2.23.



Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC001	105	105	555	4,700	10,472	10.47	79,700	8,420	7,550	22,700	258,000
LTAC002	0	3	1,090	4,150	9,246	9.25	51,000	5,270	4,380	13,100	161,000
LTAC002	90	90	828	4,730	10,538	10.54	64,700	6,930	5,820	17,500	204,000
LTAC002	96	96	454	5,170	11,519	11.52	89,300	9,420	8,400	25,200	284,000
LTAC002	99	99	560	4,670	10,405	10.41	81,600	8,420	7,630	22,900	261,000
LTAC002	102	102	450	5,070	11,296	11.30	87,500	9,250	8,310	24,900	288,000
LTAC003	54	54	646	4,770	10,628	10.63	81,900	7,810	6,310	18,900	257,000
LTAC003	93	93	617	4,430	9,870	9.87	78,800	8,420	7,040	21,100	255,000
LTAC003	96	96	605	4,430	9,870	9.87	76,000	8,300	7,010	21,000	252,000
LTAC003	99	99	609	4,370	9,736	9.74	78,300	8,390	6,990	21,000	251,000
LTAC004	12	12	1,120	2,210	4,924	4.92	40,400	4,100	4,010	12,000	128,000
LTAC004	96	96	601	4,340	9,670	9.67	78,600	8,500	7,290	21,900	257,000
LTAC004	99	99	662	4,160	9,268	9.27	77,100	8,220	7,050	21,200	244,000
LTAC004	102	102	624	4,130	9,202	9.20	73,600	8,100	7,000	21,000	246,000
LTAC004	108	108	575	4,410	9,825	9.83	80,400	8,400	7,290	21,900	258,000
LTAC005	75	75	700	3,580	7,976	7.98	67,700	7,210	6,460	19,400	216,000
LTAC005	90	90	692	3,750	8,355	8.36	69,400	7,560	6,700	20,100	225,000
LTAC005	93	93	600	4,070	9,068	9.07	74,200	8,190	7,150	21,500	249,000
LTAC005	99	99	584	4,230	9,424	9.42	74,400	8,390	7,100	21,300	253,000
LTAC005	102	102	610	4,030	8,979	8.98	70,300	8,070	6,930	20,800	248,000
LTAC006	87	87	576	4,890	10,895	10.90	78,800	8,010	6,450	19,400	273,000
LTAC006	90	90	579	4,480	9,981	9.98	77,300	8,490	6,890	20,700	258,000
LTAC006	93	93	593	4,480	9,981	9.98	78,400	8,410	7,080	21,200	257,000
LTAC006	96	96	583	4,510	10,048	10.05	75,300	8,460	7,060	21,200	259,000
LTAC007	90	90	586	4,480	9,981	9.98	76,800	8,090	7,240	21,700	255,000
LTAC007	93	93	582	4,490	10,004	10.00	77,200	8,030	7,290	21,900	252,000
LTAC007	99	99	589	4,360	9,714	9.71	73,900	7,930	6,990	21,000	252,000
LTAC007	102	102	581	4,410	9,825	9.83	75,000	8,080	7,220	21,700	271,000
LTAC008	75	75	589	4,390	9,781	9.78	75,400	8,280	6,970	20,900	256,000
LTAC008	81	81	597	4,300	9,580	9.58	75,000	8,200	6,880	20,600	253,000
LTAC008	99	99	639	4,020	8,957	8.96	72,300	7,760	6,560	19,700	261,000
LTAC008	105	105	621	4,160	9,268	9.27	73,300	7,880	6,760	20,300	249,000
LTAC008	108	108	618	4,250	9,469	9.47	75,900	8,120	7,130	21,400	250,000
LTAC008	111	111	621	4,170	9,291	9.29	73,000	8,060	6,740	20,200	255,000
LTAC008	114	114	640	4,140	9,224	9.22	75,200	7,890	6,780	20,300	263,000
LTAC008	117	117	643	4,120	9,179	9.18	75,000	7,790	6,680	20,000	260,000
LTAC009	72	72	578	4,230	9,424	9.42	73,600	8,240	7,020	21,100	256,000
LTAC009	75	75	595	4,250	9,469	9.47	75,800	8,220	7,080	21,200	269,000
LTAC009	78	78	587	4,260	9,491	9.49	74,200	8,300	6,920	20,800	269,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC009	81	81	564	4,370	9,736	9.74	76,000	8,710	7,360	22,100	267,000
LTAC009	87	87	589	4,280	9,536	9.54	75,100	8,510	7,310	21,900	260,000
LTAC009	90	90	596	4,240	9,447	9.45	75,600	8,300	7,070	21,200	254,000
LTAC009	96	96	596	4,220	9,402	9.40	75,500	8,270	6,790	20,400	256,000
LTAC009	105	105	543	4,390	9,781	9.78	81,900	8,750	7,350	22,100	265,000
LTAC010	120	120	515	4,440	9,892	9.89	81,300	9,160	7,630	22,900	272,000
LTAC010	126	126	529	4,440	9,892	9.89	80,300	9,180	7,900	23,700	269,000
LTAC011	15	15	539	4,230	9,424	9.42	77,600	7,960	7,090	21,300	250,000
LTAC011	72	72	618	4,250	9,469	9.47	73,200	8,120	6,710	20,100	251,000
LTAC011	81	81	636	4,250	9,469	9.47	74,800	8,140	6,870	20,600	249,000
LTAC012	75	75	668	4,160	9,268	9.27	73,800	7,780	6,580	19,700	242,000
LTAC012	78	78	674	4,180	9,313	9.31	73,600	8,060	6,690	20,100	243,000
LTAC012	81	81	562	4,430	9,870	9.87	80,300	8,520	6,970	20,900	262,000
LTAC012	96	96	645	4,150	9,246	9.25	72,400	7,860	6,670	20,000	247,000
LTAC012	99	99	672	4,140	9,224	9.22	74,900	7,810	6,490	19,500	245,000
LTAC012	105	105	626	4,340	9,670	9.67	77,900	8,180	6,890	20,700	254,000
LTAC012	108	108	554	4,480	9,981	9.98	81,100	8,680	7,070	21,200	269,000
LTAC012	114	114	680	4,130	9,202	9.20	73,700	7,790	6,440	19,300	243,000
LTAC012	120	120	681	4,110	9,157	9.16	73,800	7,770	6,510	19,500	242,000
LTAC014	36	36	520	4,990	11,118	11.12	81,300	8,740	7,640	22,900	270,000
LTAC014	51	51	555	4,630	10,316	10.32	77,900	8,260	7,450	22,400	270,000
LTAC014	60	60	555	4,520	10,071	10.07	77,800	8,150	7,380	22,100	260,000
LTAC014	99	99	536	4,670	10,405	10.41	79,200	8,750	8,050	24,200	268,000
LTAC015	60	60	482	5,110	11,385	11.39	84,400	9,010	8,310	24,900	280,000
LTAC015	84	84	517	4,750	10,583	10.58	81,700	8,890	8,260	24,800	271,000
LTAC015	87	87	544	4,710	10,494	10.49	79,400	8,610	8,170	24,500	265,000
LTAC015	90	90	455	4,910	10,939	10.94	86,500	9,110	8,620	25,900	285,000
LTAC015	93	93	536	4,630	10,316	10.32	81,800	8,580	8,130	24,400	264,000
LTAC016	99	99	458	4,900	10,917	10.92	88,500	9,430	8,460	25,400	285,000
LTAC016	102	102	482	4,920	10,962	10.96	89,900	9,580	8,670	26,000	286,000
LTAC016	117	117	517	4,620	10,293	10.29	81,400	9,000	7,800	23,400	274,000
LTAC016	123	123	495	4,680	10,427	10.43	88,900	9,090	8,100	24,300	276,000
LTAC016	126	126	495	4,510	10,048	10.05	81,900	8,780	7,930	23,800	271,000
LTAC016	129	129	499	4,560	10,160	10.16	83,200	8,590	8,010	24,000	271,000
LTAC018	72	72	565	4,270	9,522	9.52	82,300	8,820	7,320	22,000	267,000
LTAC018	75	75	553	4,260	9,500	9.50	81,600	8,650	7,150	21,500	267,000
LTAC018	78	78	564	4,230	9,433	9.43	79,400	8,680	7,290	21,900	267,000
LTAC018	81	81	558	4,410	9,834	9.83	84,400	9,120	7,680	23,000	271,000
LTAC018	84	84	569	4,290	9,567	9.57	85,500	8,910	7,530	22,600	269,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC018	87	87	561	4,330	9,656	9.66	84,100	8,720	7,440	22,300	269,000
LTAC018	90	90	547	4,200	9,366	9.37	82,600	8,540	7,230	21,700	265,000
LTAC018	93	93	548	4,270	9,522	9.52	83,900	8,680	7,590	22,800	268,000
LTAC018	99	99	548	4,130	9,210	9.21	80,100	8,370	7,370	22,100	264,000
LTAC018	102	102	543	4,220	9,411	9.41	82,700	8,640	7,300	21,900	269,000
LTAC018	105	105	470	4,270	9,522	9.52	83,400	8,680	7,590	22,800	283,000
LTAC018	111	111	502	4,210	9,388	9.39	83,900	8,590	8,040	24,100	275,000
LTAC018	114	114	533	4,160	9,277	9.28	83,500	8,540	7,760	23,300	268,000
LTAC018	117	117	513	4,240	9,455	9.46	82,000	8,560	7,760	23,300	272,000
LTAC018	120	120	549	4,160	9,277	9.28	82,400	8,460	7,660	23,000	265,000
LTAC018	123	123	535	4,170	9,299	9.30	81,500	8,630	7,830	23,500	270,000
LTAC018	126	126	525	4,220	9,411	9.41	82,400	8,770	7,730	23,200	272,000
LTAC019	42	42	553	4,330	9,656	9.66	85,900	9,030	7,760	23,300	269,000
LTAC019	45	45	576	4,160	9,277	9.28	78,900	8,790	6,960	20,900	263,000
LTAC019	48	48	553	4,260	9,500	9.50	83,200	8,830	7,320	22,000	271,000
LTAC019	66	66	552	4,240	9,455	9.46	81,600	8,680	7,660	23,000	268,000
LTAC019	69	69	540	4,260	9,500	9.50	83,400	8,570	7,510	22,500	268,000
LTAC019	72	72	549	4,180	9,321	9.32	81,600	8,670	7,590	22,800	267,000
LTAC019	75	75	549	4,220	9,411	9.41	82,100	8,590	7,840	23,500	268,000
LTAC019	78	78	545	4,230	9,433	9.43	82,700	8,670	7,450	22,400	267,000
LTAC019	81	81	560	4,270	9,522	9.52	81,500	8,790	7,480	22,400	267,000
LTAC019	87	87	532	4,180	9,321	9.32	76,900	7,960	7,360	22,100	262,000
LTAC019	90	90	537	4,210	9,388	9.39	83,700	8,470	7,870	23,600	264,000
LTAC019	93	93	542	3,980	8,875	8.88	79,700	8,240	7,220	21,700	264,000
LTAC019	96	96	544	3,980	8,875	8.88	79,200	8,380	7,430	22,300	263,000
LTAC019	99	99	551	4,040	9,009	9.01	79,700	8,460	7,600	22,800	261,000
LTAC019	102	102	557	4,030	8,987	8.99	80,700	8,530	7,870	23,600	262,000
LTAC019	105	105	532	3,950	8,809	8.81	78,900	8,150	7,420	22,300	263,000
LTAC019	108	108	558	4,050	9,032	9.03	82,600	8,600	7,700	23,100	262,000
LTAC019	111	111	556	4,060	9,054	9.05	84,000	8,700	8,020	24,100	263,000
LTAC019	117	117	554	4,040	9,009	9.01	81,300	8,590	8,040	24,100	265,000
LTAC019	120	120	552	4,090	9,121	9.12	82,000	8,660	7,740	23,200	263,000
LTAC019	123	123	524	4,140	9,232	9.23	79,600	8,430	7,520	22,600	265,000
LTAC019	126	126	546	4,110	9,165	9.17	80,200	8,470	7,570	22,700	264,000
LTAC019	129	129	549	4,150	9,255	9.26	80,100	8,600	7,600	22,800	265,000
LTAC020	72	72	551	4,430	9,879	9.88	83,300	8,780	7,710	23,100	270,000
LTAC022	99	99	497	4,330	9,656	9.66	82,800	8,790	8,510	25,500	273,000
LTAC022	111	111	468	4,490	10,013	10.01	86,200	9,080	9,070	27,200	281,000
LTAC022	117	117	498	4,470	9,968	9.97	88,900	9,170	8,940	26,800	278,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC022	126	126	503	4,350	9,701	9.70	84,100	8,890	8,740	26,200	274,000
LTAC023	105	105	557	4,200	9,366	9.37	77,900	8,460	8,900	26,700	N/A
LTAC023	108	108	544	4,170	9,299	9.30	78,800	8,510	8,860	26,600	258,000
LTAC024	102	102	520	4,220	9,411	9.41	75,700	8,360	8,570	25,700	263,000
LTAC024	108	108	547	4,350	9,701	9.70	80,700	8,760	8,590	25,800	264,000
LTAC025	102	102	428	4,940	11,016	11.02	86,900	9,770	10,300	30,900	287,000
LTAC025	105	105	443	4,780	10,659	10.66	81,800	9,270	9,500	28,500	282,000
LTAC025	106	106	491	4,680	10,436	10.44	81,100	8,960	9,220	27,700	272,000
LTAC026	0.3	0.3	458	5,030	11,217	11.22	78,900	9,020	8,380	25,100	276,000
LTAC026	96	96	459	4,730	10,548	10.55	80,700	9,400	9,780	29,300	276,000
LTAC026	99	99	493	4,570	10,191	10.19	81,200	9,240	9,780	29,300	271,000
LTAC026	108	108	478	4,520	10,080	10.08	81,600	9,090	9,410	28,200	269,000
LTAC027	87	87	467	4,620	10,303	10.30	79,500	8,910	9,300	27,900	273,000
LTAC027	90	90	479	4,660	10,392	10.39	83,500	9,150	9,300	27,900	271,000
LTAC027	93	93	489	4,700	10,481	10.48	84,200	9,170	9,500	28,500	271,000
LTAC027	96	96	438	4,850	10,816	10.82	87,200	9,410	9,780	29,300	285,000
LTAC027	102	102	483	4,660	10,392	10.39	81,100	9,140	9,410	28,200	274,000
LTAC027	104	104	478	4,650	10,370	10.37	82,800	8,980	9,300	27,900	271,000
LTAC028	102	102	520	4,480	9,990	9.99	77,200	9,020	9,410	28,200	265,000
LTAC028	105	105	498	4,460	9,946	9.95	78,200	8,890	9,270	27,800	265,000
LTAC029	75	75	458	4,820	10,749	10.75	88,200	9,300	9,150	27,500	286,000
LTAC029	78	78	456	4,740	10,570	10.57	85,500	9,130	9,280	27,800	282,000
LTAC029	81	81	475	4,710	10,503	10.50	83,800	9,170	9,030	27,100	280,000
LTAC029	84	84	444	4,580	10,213	10.21	78,600	8,670	8,630	25,900	276,000
LTAC029	87	87	447	4,730	10,548	10.55	84,700	9,050	9,580	28,700	281,000
LTAC029	90	90	463	4,560	10,169	10.17	82,400	8,840	8,770	26,300	278,000
LTAC029	93	93	452	4,660	10,392	10.39	84,400	8,930	9,220	27,700	280,000
LTAC029	99	99	452	4,700	10,481	10.48	85,600	8,880	9,410	28,200	280,000
LTAC030	81	81	453	4,660	10,392	10.39	85,700	8,790	9,010	27,000	262,000
LTAC030	84	84	535	4,280	9,544	9.54	75,900	8,410	8,820	26,500	254,000
LTAC030	87	87	549	4,290	9,567	9.57	75,800	8,760	8,500	25,500	259,000
LTAC030	90	90	526	4,360	9,723	9.72	76,100	8,400	8,910	26,700	259,000
LTAC031	102	102	534	4,150	9,255	9.26	77,700	8,320	8,340	25,000	258,000
LTAC031	105	105	547	4,070	9,076	9.08	75,000	8,080	8,340	25,000	254,000
LTAC032	84	84	462	4,660	10,392	10.39	86,000	8,830	8,880	26,600	279,000
LTAC032	87	87	469	4,650	10,370	10.37	83,300	8,760	8,700	26,100	281,000
LTAC032	96	96	479	4,620	10,303	10.30	84,600	8,650	8,630	25,900	278,000
LTAC032	99	99	483	4,800	10,704	10.70	88,300	9,200	9,600	28,800	284,000
LTAC032	102	102	479	4,810	10,726	10.73	86,600	9,020	9,060	27,200	281,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC033	87	87	456	4,930	10,994	10.99	83,400	9,150	9,600	28,800	284,000
LTAC033	90	90	431	4,970	11,083	11.08	87,300	9,450	10,100	30,300	292,000
LTAC033	93	93	425	4,710	10,503	10.50	83,200	9,050	9,130	27,400	279,000
LTAC033	95	95	485	4,970	11,083	11.08	82,600	8,040	8,500	25,500	270,000
LTAC034	78	78	479	4,630	10,325	10.33	84,800	8,550	8,650	26,000	274,000
LTAC034	102	102	506	4,530	10,102	10.10	81,200	8,610	8,260	24,800	273,000
LTAC035	93	93	509	4,680	10,436	10.44	82,800	9,140	8,450	25,400	279,000
LTAC035	99	99	509	4,680	10,436	10.44	82,800	9,140	8,450	25,400	279,000
LTAC035	106	106	509	4,680	10,436	10.44	82,800	9,140	8,450	25,400	279,000
LTAC034	90	90	509	4,680	10,436	10.44	82,800	9,140	8,450	25,400	279,000
LTAC034	96	96	509	4,680	10,436	10.44	82,800	9,140	8,450	25,400	279,000
LTAC034	99	99	510	4,610	10,280	10.28	83,600	8,700	8,260	24,800	276,000
LTAC034	102	102	511	4,640	10,347	10.35	83,000	8,870	8,330	25,000	279,000
LTAC034	105	105	543	4,660	10,392	10.39	83,500	9,300	8,510	25,500	279,000
LTAC034	108	108	504	4,650	10,370	10.37	83,900	8,700	8,250	24,800	274,000
LTAC037	75	75	480	4,850	10,816	10.82	86,900	9,160	8,640	25,900	286,000
LTAC037	78	78	454	4,690	10,459	10.46	82,700	8,610	8,260	24,800	282,000
LTAC037	81	81	475	4,860	10,838	10.84	85,000	9,020	8,480	25,400	282,000
LTAC037	84	84	478	4,750	10,593	10.59	81,400	8,790	8,300	24,900	280,000
LTAC037	87	87	486	4,780	10,659	10.66	86,400	8,920	8,650	26,000	276,000
LTAC037	90	90	501	4,800	10,704	10.70	86,600	9,170	8,570	25,700	276,000
LTAC037	93	93	486	4,770	10,637	10.64	82,800	8,870	8,560	25,700	276,000
LTAC037	96	96	471	4,900	10,927	10.93	87,000	9,290	8,600	25,800	283,000
LTAC037	99	99	478	4,910	10,949	10.95	86,400	9,470	8,960	26,900	280,000
LTAC038	87	87	491	4,580	10,213	10.21	83,800	9,490	8,870	26,600	281,000
LTAC038	90	90	420	4,790	10,682	10.68	88,000	9,570	9,220	27,700	290,000
LTAC038	93	93	431	4,740	10,570	10.57	89,500	10,100	9,100	27,300	292,000
LTAC038	105	105	421	4,770	10,637	10.64	89,500	9,500	9,350	28,100	291,000
LTAC038	108	108	422	4,780	10,659	10.66	92,200	9,700	9,460	28,400	291,000
LTAC038	111	111	451	4,590	10,236	10.24	86,500	9,420	9,220	27,700	284,000
LTAC038	117	117	439	4,810	10,726	10.73	88,600	9,720	9,190	27,600	288,000
LTAC038	120	120	460	4,650	10,370	10.37	88,200	9,460	9,180	27,500	283,000
LTAC038	123	123	434	4,760	10,615	10.62	89,800	9,690	8,970	26,900	289,000
LTAC038	129	129	440	4,810	10,726	10.73	89,700	9,820	9,030	27,100	290,000
LTAC039	48	48	563	4,340	9,678	9.68	77,400	8,150	7,580	22,700	250,000
LTAC040	99	99	361	5,800	12,934	12.93	95,800	11,200	10,100	30,300	319,000
LTAC040	105	105	458	4,750	10,593	10.59	83,600	8,860	8,280	24,800	275,000
LTAC040	108	108	457	4,690	10,459	10.46	85,200	8,830	8,220	24,700	276,000
LTAC040	111	111	447	4,630	10,325	10.33	84,200	8,720	8,230	24,700	274,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC040	114	114	473	4,900	10,927	10.93	88,200	9,220	8,710	26,100	283,000
LTAC040	117	117	458	4,780	10,659	10.66	87,500	8,980	8,220	24,700	277,000
LTAC040	120	120	462	4,820	10,749	10.75	86,000	9,070	8,130	24,400	277,000
LTAC040	126	126	466	4,870	10,860	10.86	85,700	9,080	8,360	25,100	277,000
LTAC040	129	129	459	4,760	10,615	10.62	86,700	9,040	8,440	25,300	276,000
LTAC040	131	131	463	4,800	10,704	10.70	84,800	9,020	8,170	24,500	276,000
LTAC041	72	72	516	4,670	10,414	10.41	85,500	8,830	8,110	24,300	269,000
LTAC041	75	75	505	4,720	10,526	10.53	83,800	8,690	8,110	24,300	272,000
LTAC041	78	78	498	4,630	10,325	10.33	82,100	8,550	7,880	23,600	268,000
LTAC041	81	81	493	4,700	10,481	10.48	85,600	8,530	8,080	24,200	270,000
LTAC041	84	84	517	4,570	10,191	10.19	83,600	8,530	8,310	24,900	262,000
LTAC041	87	87	532	4,640	10,347	10.35	82,400	8,950	8,460	25,400	267,000
LTAC042	78	78	463	4,880	10,882	10.88	82,200	8,320	8,030	24,100	271,000
LTAC042	81	81	509	4,800	10,704	10.70	81,000	9,080	8,290	24,900	270,000
LTAC042	84	84	445	4,730	10,548	10.55	79,600	7,980	8,090	24,300	268,000
LTAC042	87	87	444	4,780	10,659	10.66	81,900	8,100	7,970	23,900	272,000
LTAC042	90	90	444	4,830	10,771	10.77	82,800	8,140	8,130	24,400	271,000
LTAC042	93	93	455	4,940	11,016	11.02	85,900	8,420	8,220	24,700	271,000
LTAC042	96	96	457	4,770	10,637	10.64	81,700	8,380	8,280	24,800	272,000
LTAC042	99	99	458	4,690	10,459	10.46	80,900	8,450	8,040	24,100	276,000
LTAC043	90	90	512	4,680	10,436	10.44	85,100	8,650	8,320	25,000	272,000
LTAC043	99	99	482	4,670	10,414	10.41	85,200	8,610	8,270	24,800	276,000
LTAC043	105	105	467	4,660	10,392	10.39	86,100	8,770	8,370	25,100	279,000
LTAC043	108	108	463	4,670	10,414	10.41	86,800	8,690	8,550	25,700	280,000
LTAC043	111	111	461	4,650	10,370	10.37	86,600	8,710	8,290	24,900	278,000
LTAC043	114	114	473	4,650	10,370	10.37	85,400	8,740	8,320	25,000	278,000
LTAC043	117	117	479	4,810	10,726	10.73	88,100	8,920	8,380	25,100	279,000
LTAC043	120	120	470	4,700	10,481	10.48	85,800	8,860	8,670	26,000	278,000
LTAC043	123	123	464	4,650	10,370	10.37	81,400	8,550	8,350	25,100	277,000
LTAC043	126	126	469	4,730	10,548	10.55	87,800	8,720	8,460	25,400	279,000
LTAC043	132	132	468	4,760	10,615	10.62	85,400	8,670	8,520	25,600	281,000
LTAC043	135	135	459	4,760	10,615	10.62	84,000	8,540	8,380	25,100	278,000
LTAC043	141	141	482	4,690	10,459	10.46	84,200	8,690	8,570	25,700	279,000
LTAC044	90	90	575	4,230	9,433	9.43	81,800	8,510	7,530	22,600	264,000
LTAC044	93	93	560	4,170	9,299	9.30	80,900	8,310	7,700	23,100	262,000
LTAC044	96	96	530	4,110	9,165	9.17	80,900	8,220	7,340	22,000	264,000
LTAC044	99	99	550	4,090	9,121	9.12	81,700	8,300	7,590	22,800	265,000
LTAC044	102	102	530	4,100	9,143	9.14	80,900	8,290	7,660	23,000	265,000
LTAC045	75	75	578	4,550	10,147	10.15	83,200	8,100	7,700	23,100	267,000

Hole ID	From	To	Ca	K	SOP equiv. <sup>2</sup>		Na	Mg	S	SO <sub>4</sub>	TDS
	(m)	(m)	(mg/L)	(mg/L)	(mg/L)	(kg/m <sup>3</sup> )	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
LTAC048	87	87	526	4,340	9,678	9.68	83,200	8,700	8,080	24,200	269,000
LTAC048	90	90	514	4,370	9,745	9.75	82,700	8,790	8,010	24,000	271,000
LTAC048	93	93	551	4,350	9,701	9.70	81,100	8,770	7,980	23,900	273,000
LTAC048	96	96	528	4,320	9,634	9.63	83,100	8,360	8,100	24,300	271,000
LTAC048	114	114	494	4,340	9,678	9.68	83,700	8,730	7,890	23,700	277,000
LTAC048	117	117	514	4,260	9,500	9.50	83,000	8,550	8,010	24,000	271,000
LTAC049	99	99	524	4,320	9,634	9.63	80,000	8,520	8,170	24,500	266,000
LTAC049	105	105	549	4,310	9,611	9.61	82,100	8,740	8,390	25,200	265,000
LTAC049	108	108	550	4,390	9,790	9.79	87,400	8,830	8,580	25,700	268,000
LTAC049	117	117	570	4,370	9,745	9.75	80,900	9,070	8,790	26,400	268,000
LTAC049	125	125	534	4,310	9,611	9.61	78,600	8,500	8,080	24,200	265,000
LTAC050	96	96	529	4,310	9,611	9.61	82,400	9,040	8,260	24,800	272,000
LTAC050	99	99	507	4,340	9,678	9.68	84,900	8,950	8,360	25,100	272,000
LTAC052	69	69	497	4,760	10,615	10.62	83,800	8,710	7,770	23,300	284,000
LTAC052	84	84	517	4,850	10,816	10.82	89,800	8,930	8,120	24,400	285,000
LTAC052	87	87	510	4,960	11,061	11.06	88,700	8,930	8,280	24,800	288,000
LTAC053	83	83	535	4,880	10,882	10.88	85,000	8,210	7,200	21,600	281,000
LTAC054	105	105	476	4700	10,481	10.48	83,600	8,690	8,130	24,400	278,000

Lake Throssell PSD Analysis Results

Hole ID	Depth (m)		% Sand	% Silt	% Clay	Stratigraphy	Specific Yield (%)	Saturated Hydraulic Conductivity (m/d)
	From	To						
LTAC017	59	68	64	31	4	Lacustrine Clay	19	0.61
LTAC036	87	90	47	44	9	Lacustrine Clay	12	0.15
LTAC043	87	90	13	81	5	Lacustrine Clay	3	0.01
LTAC043	90	93	54	31	16	Lacustrine Clay	11	0.09
LTAC019	69	77	80	16	4	Basal Sand	24	1.02
LTAC043	96	99	83	9	8	Basal Sand	23	0.67
LTAC043	99	102	86	6	8	Basal Sand	23	0.73
LTAC049	96	99	84	9	6	Basal Sand	25	0.91
LTAC050	93	96	64	28	8	Basal Sand	17	0.35
LTAC050	96	99	86	9	5	Basal Sand	26	1.12
LTAC027	90	93	88	5	7	Glacial Fluvial	25	0.90
LTAC027	93	96	94	4	2	Glacial Fluvial	32	4.36
LTAC027	99	102	83	3	13	Glacial Fluvial	19	0.36
LTAC033	84	87	69	26	6	Glacial Fluvial	20	0.63
LTAC033	87	90	38	56	6	Glacial Fluvial	11	0.13
LTAC033	90	93	54	36	10	Glacial Fluvial	14	0.19
LTAC033	93	95	65	27	8	Glacial Fluvial	18	0.39
LTAC035	96	99	81	16	3	Glacial Fluvial	26	1.33
LTAC035	103	106	71	20	9	Glacial Fluvial	19	0.44
LTAC036	93	96	83	10	7	Glacial Fluvial	23	0.73
LTAC036	96	99	76	16	8	Glacial Fluvial	21	0.55
LTAC036	99	102	62	26	12	Glacial Fluvial	15	0.20
LTAC036	105	108	55	35	10	Glacial Fluvial	14	0.20
LTAC036	108	111	55	32	13	Glacial Fluvial	13	0.14

Hole ID	Depth (m)		% Sand	% Silt	% Clay	Stratigraphy	Specific Yield (%)	Saturated Hydraulic Conductivity (m/d)
	From	To						
LTAC038	84	87	77	14	9	Glacial Fluvial	20	0.49
LTAC038	102	105	84	9	6	Glacial Fluvial	24	0.87
LTAC038	108	111	55	34	11	Glacial Fluvial	13	0.16
LTAC038	117	120	67	26	7	Glacial Fluvial	19	0.46
LTAC038	123	126	73	15	12	Glacial Fluvial	17	0.30
LTAC040	96	99	88	8	4	Glacial Fluvial	27	1.25
LTAC040	102	105	89	5	5	Glacial Fluvial	27	1.17
LTAC040	105	108	77	5	18	Glacial Fluvial	15	0.17
LTAC040	108	111	82	7	11	Glacial Fluvial	20	0.48
LTAC040	111	114	85	5	10	Glacial Fluvial	22	0.59
LTAC040	114	117	68	20	12	Glacial Fluvial	16	0.27
LTAC040	117	120	64	24	11	Glacial Fluvial	16	0.25
LTAC040	120	123	76	13	10	Glacial Fluvial	19	0.42
LTAC040	123	126	55	30	15	Glacial Fluvial	12	0.11
LTAC040	126	129	70	15	15	Glacial Fluvial	14	0.18
LTAC040	129	132	76	10	14	Glacial Fluvial	17	0.28
LTAC042	75	78	73	20	7	Glacial Fluvial	21	0.61
LTAC042	78	81	84	10	5	Glacial Fluvial	25	1.04
LTAC042	81	84	86	9	5	Glacial Fluvial	26	1.12
LTAC042	84	87	87	6	7	Glacial Fluvial	25	0.89
LTAC042	87	90	82	11	7	Glacial Fluvial	24	0.83
LTAC042	90	93	70	23	7	Glacial Fluvial	20	0.54
LTAC042	93	96	74	15	11	Glacial Fluvial	18	0.37
LTAC042	96	99	80	11	9	Glacial Fluvial	22	0.59
LTAC043	105	108	69	20	11	Glacial Fluvial	17	0.29
LTAC043	108	111	46	47	8	Glacial Fluvial	12	0.16
LTAC043	117	120	63	28	9	Glacial Fluvial	17	0.32
LTAC043	120	123	51	37	12	Glacial Fluvial	12	0.13
LTAC043	123	126	49	39	12	Glacial Fluvial	12	0.12
LTAC043	126	129	68	26	6	Glacial Fluvial	20	0.55
LTAC043	129	132	46	42	12	Glacial Fluvial	11	0.10
LTAC043	132	135	60	30	10	Glacial Fluvial	15	0.25
LTAC043	135	138	48	40	12	Glacial Fluvial	11	0.10
LTAC043	138	141	44	41	14	Glacial Fluvial	10	0.07
LTAC035	90	93	39	55	6	Perm Saprolite	11	0.14
LTAC049	105	108	51	37	12	Perm Saprolite	12	0.13
LTAC049	114	117	39	50	10	Perm Saprolite	10	0.08
LTAC049	123	126	39	50	11	Perm Saprolite	9	0.07



## APPENDIX 2 – JORC Table 1 (Lake Throssell July 2021 Resource Update)

Section 1: Sampling Techniques and Data		
Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> <li>Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.</li> <li>Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.</li> <li>Aspects of the determination of mineralisation that are Material to the Public Report.</li> <li>In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.</li> </ul>	<ul style="list-style-type: none"> <li>During aircore drilling brine sampling was carried out via airlifting during drilling at specific depths governed by the geology and brine inflow encountered. Brine samples were collected in a bucket, with approximate flow rates measured during sample collection. Fine sediment was allowed to settle prior to the brine sample being collected by decanting from the top of the bucket.</li> <li>Brine samples from aircore drilling are considered indicative of the zone directly above the current drill depth, but maybe skewed due the geology and potential for minor volumes to flow down hole in low permeability zones.</li> <li>Geological core samples were collected during the heli-rotary auger program using Lexan tubes at specific intervals.</li> <li>Brine samples were collected from bailing the auger hole at known intervals.</li> <li>A hand auger was used to complete holes to the target depth of ~1.2 metres. The brine was allowed to stand for several minutes to allow fine suspended sediment to settle. The final sample was obtained by decanting from the top of the water column.</li> </ul>
Drilling techniques	<ul style="list-style-type: none"> <li>Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).</li> </ul>	<ul style="list-style-type: none"> <li>Lake Throssell air-core drilling was at 3.5" diameter.</li> <li>The rotary auger holes were drilled at 7" hollow stem.</li> <li>Hand auger holes were augered with 8" solid flight augers.</li> <li>All holes were drilled vertically.</li> </ul>
Drill sample recovery	<ul style="list-style-type: none"> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<ul style="list-style-type: none"> <li>Lithological sample recovery was very good from air core drilling, indicated by large piles of lithological sample with little contamination.</li> <li>Lexan tube recovery was near &gt;90%.</li> </ul>
Geologic Logging	<ul style="list-style-type: none"> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	<ul style="list-style-type: none"> <li>All geological samples collected during all forms of drilling are qualitatively logged by a qualified geologist at 1m intervals, to gain an understanding of the variability in aquifer materials hosting the brine.</li> <li>Geological logging and other hydrogeological parameter data is recorded within a database.</li> </ul>

Section 1: Sampling Techniques and Data		
Criteria	JORC Code explanation	Commentary
		<ul style="list-style-type: none"> <li>Drilling lithological samples are washed and stored in chip trays for future reference.</li> </ul>
Subsampling techniques and sample preparation	<ul style="list-style-type: none"> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</li> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/ second-half sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	<ul style="list-style-type: none"> <li>No sample results are reported.</li> <li>Core samples from the hollow auger drilling were collected at various intervals using Lexan tubes.</li> <li>All samples have been stored in core trays and secured for transport back to Perth.</li> <li>Core plugs have been taken by cutting the lexan tubes and taking a vertical plug through the centre of the core. All samples were frozen in dry ice prior to trimming and then length and diameter were measured to calculate bulk volume. All samples were kept frozen in dry ice prior then mounted in Nickel sleeving with screens at each end to prevent material loss.</li> </ul>
Quality of assay data and laboratory tests	<ul style="list-style-type: none"> <li>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</li> <li>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</li> <li>Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.</li> </ul>	<ul style="list-style-type: none"> <li>All samples are being submitted to Bureau Veritas Pty Ltd in Perth for analysis.</li> <li>Brine samples (250ml bottles) have been submitted for determination of Ca, Mg, K and S (as SO<sub>4</sub>) via ICP-AES analysis.</li> <li>Other parameters including TDS (Gravimetric), pH, chloride and SG will also be determined.</li> <li>Selected samples have also been submitted for a comprehensive multi-element suite via ICP-MS determination.</li> <li>Field duplicates have been collected and lab repeats completed at a rate of 1 in 10 samples for QA/QC purposes.</li> <li>All QA/QC stats are within acceptable limits for an Inferred Resource.</li> </ul>
Verification of sampling and assaying	<ul style="list-style-type: none"> <li>The verification of significant intersections by either independent or alternative company personnel.</li> <li>The use of twinned holes.</li> <li>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</li> <li>Discuss any adjustment to assay data.</li> </ul>	<ul style="list-style-type: none"> <li>The assay data remains unadjusted.</li> </ul>
Location of data points	<ul style="list-style-type: none"> <li>Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.</li> <li>Specification of the grid system used.</li> <li>Quality and adequacy of topographic control.</li> </ul>	<ul style="list-style-type: none"> <li>Hole location coordinates obtained by handheld GPS.</li> <li>The grid system used was MGA94, Zone 51.</li> </ul>
Data spacing and distribution	<ul style="list-style-type: none"> <li>Data spacing for reporting of Exploration Results.</li> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> </ul>	<ul style="list-style-type: none"> <li>Drilling to date in the surface sediments has resulted in an average drill spacing of approximately 1.5km, with a maximum separation of 3.5km.</li> <li>Drilling to date in the deep palaeovalley has resulted in nominal drill hole spacing of between 200-1,000m along drill</li> </ul>

Section 1: Sampling Techniques and Data		
Criteria	JORC Code explanation	Commentary
	<ul style="list-style-type: none"> <li>Whether sample compositing has been applied.</li> </ul>	<ul style="list-style-type: none"> <li>transects and between 3-5km along strike.</li> </ul>
Orientation of data in relation to geological structure	<ul style="list-style-type: none"> <li>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</li> <li>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</li> </ul>	<ul style="list-style-type: none"> <li>Not applicable, considering the deposit type.</li> <li>All drill holes are vertical.</li> </ul>
Sample security	<ul style="list-style-type: none"> <li>The measures taken to ensure sample security.</li> </ul>	<ul style="list-style-type: none"> <li>Samples collected during the work programs were delivered directly from site to the laboratory by field personnel.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>The results of any audits or reviews of sampling techniques and data.</li> </ul>	<ul style="list-style-type: none"> <li>None.</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> <li>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</li> <li>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</li> </ul>	<ul style="list-style-type: none"> <li>EL38/3065 is 100% owned by Trigg Mining's 100% owned subsidiary K2O Minerals Pty Ltd.</li> <li>E38/3544, E38/3483, E38/3458 and E38/3537 have been applied for by K2O Minerals Pty Ltd, a 100% owned subsidiary of Trigg Mining Limited., and are pending.</li> <li>Trigg Mining has an Exploration Access Agreement with the Ngaanyatjarra, traditional owners of the Lake Throssell area.</li> </ul>
Exploration done by other parties	<ul style="list-style-type: none"> <li>Acknowledgment and appraisal of exploration by other parties.</li> </ul>	<ul style="list-style-type: none"> <li>No previous drilling has been completed on Lake Throssell.</li> </ul>
Geology	<ul style="list-style-type: none"> <li>Deposit type, geological setting and style of mineralisation.</li> </ul>	<ul style="list-style-type: none"> <li>Shallow unconfined surficial lake playa and deep confined palaeo-drainage system as discussed in the report.</li> <li>The deposit is a brine containing potassium and sulphate ions that could form a potassium sulphate salt. The brine is contained within saturated sediments.</li> </ul>
Drill hole Information	<ul style="list-style-type: none"> <li>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:                             <ul style="list-style-type: none"> <li>easting and northing of the drill hole collar;</li> <li>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar;</li> <li>dip and azimuth of the hole;</li> <li>downhole length and interception depth; and</li> <li>hole length.</li> </ul> </li> <li>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the</li> </ul>	<ul style="list-style-type: none"> <li>Information has been included in Appendix 1.</li> <li>All holes are vertical.</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
	<i>understanding of the report, the Competent Person should clearly explain why this is the case.</i>	
Data aggregation methods	<ul style="list-style-type: none"> <li>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.</li> <li>Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</li> <li>The assumptions used for any reporting of metal equivalent values should be clearly stated.</li> </ul>	<ul style="list-style-type: none"> <li>No weighted averages are presented for exploration results.</li> <li>All brine sample intervals are stated in the brine tables.</li> <li>No cut offs have been applied.</li> </ul>
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'downhole length, true width not known').</li> </ul>	<ul style="list-style-type: none"> <li>The mineralisation appears to be continuous in the vicinity of the lake. Grade change laterally away from the lake has not been confirmed by drilling.</li> </ul>
Diagrams	<ul style="list-style-type: none"> <li>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</li> </ul>	<ul style="list-style-type: none"> <li>Refer to figures/tables in this announcement.</li> </ul>
Balanced reporting	<ul style="list-style-type: none"> <li>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</li> </ul>	<ul style="list-style-type: none"> <li>All pertinent results have been reported.</li> </ul>
Other substantive exploration data	<ul style="list-style-type: none"> <li>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</li> </ul>	<ul style="list-style-type: none"> <li>All exploration results are presented in the report.</li> <li>Bulk brine samples have been collected to commence preliminary brine and evaporation salt analysis.</li> </ul>
Further work	<ul style="list-style-type: none"> <li>The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).</li> <li>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</li> </ul>	<ul style="list-style-type: none"> <li>Lake surface trenching and test pumping to confirm aquifer properties and potential flow rates.</li> <li>Infill air-core drilling at sites identified by the geophysical surveys.</li> <li>Installation of test production bores and hydraulic testing of the aquifer to determine aquifer properties, brine</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
		<p>grade and allow estimates of sustainable pumping rates.</p> <ul style="list-style-type: none"> <li>Additional exploration on tenements as they become granted.</li> </ul>

Section 3: Estimation of Mineral Resources		
Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> <li>Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.</li> <li>Data validation procedures used.</li> </ul>	<ul style="list-style-type: none"> <li>Cross-check of laboratory assay reports and the resource database.</li> <li>Review of sample histograms used in Resource models.</li> <li>QA/QC analysis using Ionic balance and relative percent differences using duplicate samples.</li> </ul>
Site visits	<ul style="list-style-type: none"> <li>Comment on any site visits undertaken by the Competent Person and the outcome of those visits.</li> <li>If no site visits have been undertaken indicate why this is the case.</li> </ul>	<ul style="list-style-type: none"> <li>No site visits have been completed as wet weather prohibited the planned site visit in December 2020.</li> </ul>
Geological interpretation	<ul style="list-style-type: none"> <li>Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.</li> <li>Nature of the data used and of any assumptions made.</li> <li>The effect, if any, of alternative interpretations on Mineral Resource estimation.</li> <li>The use of geology in guiding and controlling Mineral Resource estimation.</li> <li>The factors affecting continuity both of grade and geology.</li> </ul>	<ul style="list-style-type: none"> <li>The resource is contained within brine hosted in Cenozoic Palaeovalley stratigraphy and the underlying weathered Permian bedrock.</li> <li>The geological model is considered adequately constrained for an Inferred Resource. Drilling transects have confirmed a geological sequence based on well understood stratigraphic depositional processes. The deposit is not structurally complex; it is alluvial fill in a palaeovalley depo-center, within a sedimentary trough. Weathering profiles within the Permian sediments have complicated geological model.</li> <li>The geological model for the saprolite of the weathered Permian is less certain. The Paterson Formation contains thick unconsolidated sand sequences derived from weathered sandstone within the Paterson Formation. The continuity and controls on these lenses are not well mapped but has been encountered in a number of the deeper exploration holes.</li> <li>The geological interpretation informs the volume of the resource host.</li> <li>Grade variability appears to be largely controlled by recharge runoff and windblown accumulation of surface water at the surface.</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
Dimensions	<ul style="list-style-type: none"> <li>The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.</li> </ul>	<ul style="list-style-type: none"> <li>The Mineral Resource extends approximately 50 km along the strike of the lake surface and palaeovalley. The depth of the model is constrained by the depth of investigation and the search parameters used.</li> <li>The thickness of the aquifer hosting the brine Mineral Resource has been based on the groundwater elevation (measured as depth below surface) and a sediment thickness above the impermeable bedrock or depth of investigation when open at depth.</li> <li>The volume of brine that can be abstracted has been based the adopted specific yields of each lithological category. The specific yields are determined from a combination of laboratory PSD analysis, core analysis and comparisons with publicly available data from equivalent geological settings.</li> </ul>
Estimation and modelling techniques	<ul style="list-style-type: none"> <li>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</li> <li>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</li> <li>The assumptions made regarding recovery of by-products.</li> <li>Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation).</li> <li>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</li> <li>Any assumptions behind modelling of selective mining units.</li> <li>Any assumptions about correlation between variables.</li> <li>Description of how the geological interpretation was used to control the resource estimates.</li> <li>Discussion of basis for using or not using grade cutting or capping.</li> <li>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</li> </ul>	<ul style="list-style-type: none"> <li>Modelling procedures and parameters are discussed in the report. Additional details are presented below were relevant.</li> <li>The Resource zone is constrained by the tenement boundaries, island parameters, search parameters and sampling intervals.</li> <li>The block model cell sizes took into account the density of the sample spacing within the Resource. The block spacing of the z direction considered the vertical variability of the brine within lithologies, increases and decreases in grade with depth are observed across lithologies therefore higher resolution z component (10m) was selected to allow for pinching geology, so this trend in grade variability can be accurately represented.</li> <li>The average sample spacing at shallow depths inclusive of test pits and auger holes is approximately 2.5km. At depths greater than 6m the average sample spacing is less than 3.5km, between transects and less than 1km along transects.</li> <li>Selective mining units have not been considered.</li> <li>There are no assumptions about correlation between variables.</li> <li>No cut-off grade has been used.</li> </ul>
Moisture	<ul style="list-style-type: none"> <li>Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.</li> </ul>	<ul style="list-style-type: none"> <li>Tonnages of potassium have been estimated on a dry, weight volume basis (%w/v). For example, 10kg SOP per cubic metre of brine.</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
<i>Cut-off parameters</i>	<ul style="list-style-type: none"> <li>The basis of the adopted cut-off grade(s) or quality parameters applied.</li> </ul>	<ul style="list-style-type: none"> <li>No grade cut-off parameters have been used.</li> </ul>
<i>Mining factors or assumptions</i>	<ul style="list-style-type: none"> <li>Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>The mining method is likely to be via pumping of brine from the aquifers by submersible bore pumps targeting the basal sand and glacial fluvial aquifers and shallow trenches targeting the surficial aquifer.</li> <li>Abstracted brine will be concentrated, crystallised and purified to produce a product which will have additional recovery factors.</li> <li>Though specific yield and total porosity provide a measure of the volume of brine present in an aquifer system hydraulic conductivity, transmissivity and confined storage controls are the main factor in defining mining factors and are addressed during Ore Reserve estimating.</li> <li>It is not possible to extract all the drainable porosity contained brine with these methods, due to the natural physical dynamics of abstraction from an aquifer.</li> <li>Ore Reserves are required to quantify the economically extractable portion of the Mineral Resources.</li> </ul>
<i>Metallurgical factors or assumptions</i>	<ul style="list-style-type: none"> <li>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>Limited metallurgical test work has been completed on the brine to confirm evaporation pathways and durations.</li> <li>Comparisons with peer group brine studies suggest that a SOP product can be obtained from the average composition of the Lake Throssell brine. However further evaporation tests and simulations are required.</li> </ul>
<i>Environmental factors or assumptions</i>	<ul style="list-style-type: none"> <li>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</li> </ul>	<ul style="list-style-type: none"> <li>In this very early stage of the project it is not possible to quantify environmental impacts. The project is assumed to have a limited, localized environmental impact, associated with minor impacts on surface disturbance associated with excavation of trenches, water quality changes of adjacent "fresher" aquifer systems, stock piling of salt by-products and potentially groundwater dependent vegetation.</li> </ul>

Section 2: Reporting of Exploration Results		
Criteria	JORC Code explanation	Commentary
Bulk density	<ul style="list-style-type: none"> <li>• Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</li> <li>• The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</li> <li>• Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</li> </ul>	<ul style="list-style-type: none"> <li>• Tonnages of potassium have been estimated on a dry, weight volume basis (%w/v). For example, 10kg SOP per cubic metre of brine.</li> <li>• As the resource is a brine, bulk density is not applicable.</li> <li>• The resource has been calculated using specific yield (drainable porosity) determined using a combination of PSD analysis, Core analysis and comparisons to publicly available data.</li> </ul>
Classification	<ul style="list-style-type: none"> <li>• The basis for the classification of the Mineral Resources into varying confidence categories.</li> <li>• Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</li> <li>• Whether the result appropriately reflects the Competent Person's view of the deposit.</li> </ul>	<ul style="list-style-type: none"> <li>• At this stage of the project an Inferred Mineral Resource is defined. The Resource Estimate is appropriate for Inferred Resources only.</li> <li>• The JORC (2012) Code including the Association of Mining and Exploration Companies (AMEC) Brine Guideline were used to determine the confidence category.</li> </ul>
Audits or reviews	<ul style="list-style-type: none"> <li>• The results of any audits or reviews of Mineral Resource estimates.</li> </ul>	<ul style="list-style-type: none"> <li>• None</li> </ul>
Discussion of relative accuracy/confidence	<ul style="list-style-type: none"> <li>• Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</li> <li>• The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</li> <li>• These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</li> </ul>	<ul style="list-style-type: none"> <li>• The Mineral Resource contains aqueous potassium, sulphate and other ions, existing as a brine in a sub-surface aquifer. The JORC code deals predominantly with solid minerals and does not deal with liquid solutions as a resource. The relative accuracy of the stated resource considers the geological and hydrogeological uncertainties of dealing with a brine.</li> <li>• The Association of Mining and Exploration Companies (AMEC) has developed guidelines to define a brine Mineral Resource and Ore Reserve. The brine specific guidance to interpretation of the JORC Code was published by AMEC and accepted by JORC in April 2019. These guidelines are adhered to in this Resource Estimate.</li> <li>• Specific yield estimates to determine drainable brine volume as the Resource Estimate is considered to be the most relevant measure of brine abstraction under reasonable prospects for eventual economic extraction.</li> </ul>